

# Development and Optimization of Multi-Functional SCR-DPF Aftertreatment for Heavy-Duty $\text{NO}_x$ and Soot Emission Reduction

**Kenneth G. Rappé**

Co-Principal Investigator

Pacific Northwest National Laboratory

**PACCAR Technical Center**

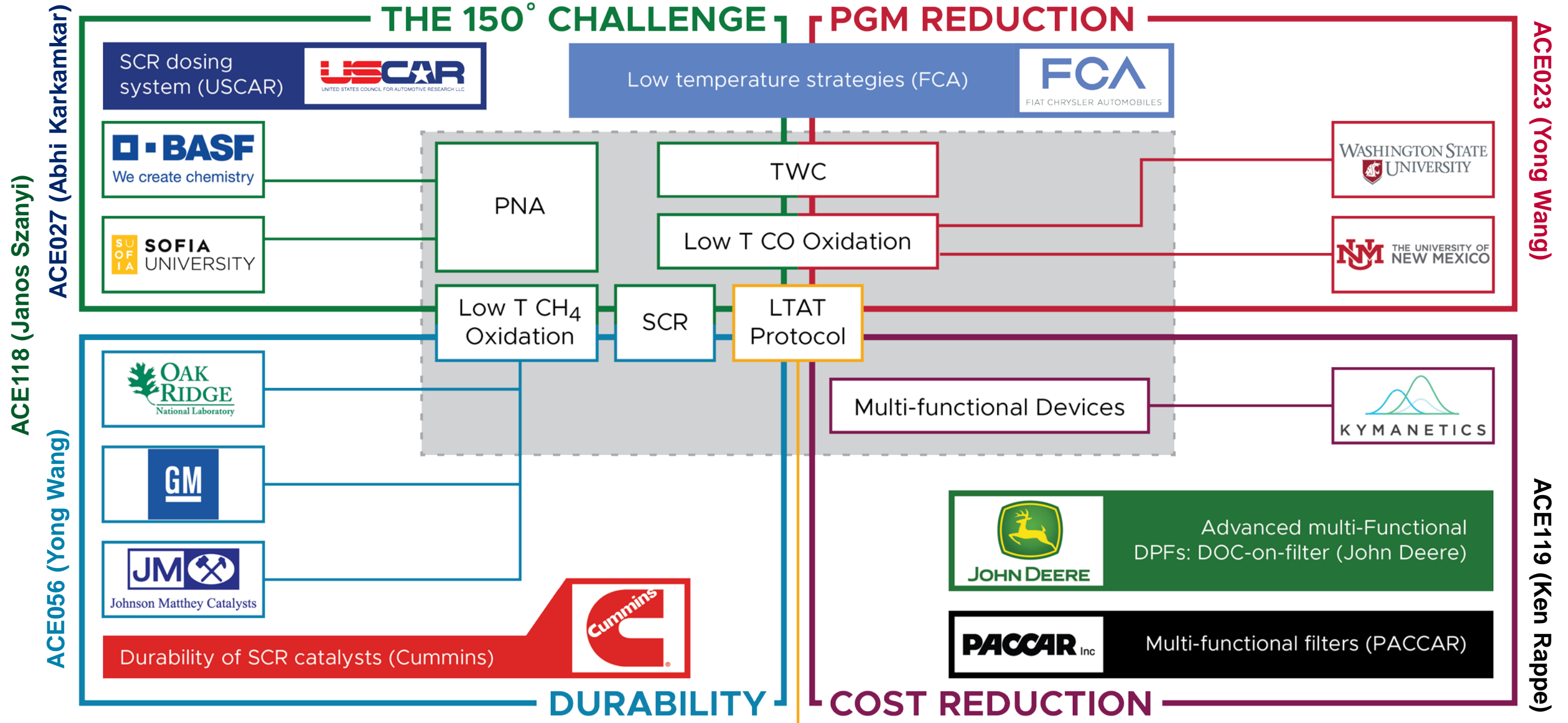
Randal Goffe (Co-PI), Cynthia Webb

**Pacific Northwest National Laboratory**

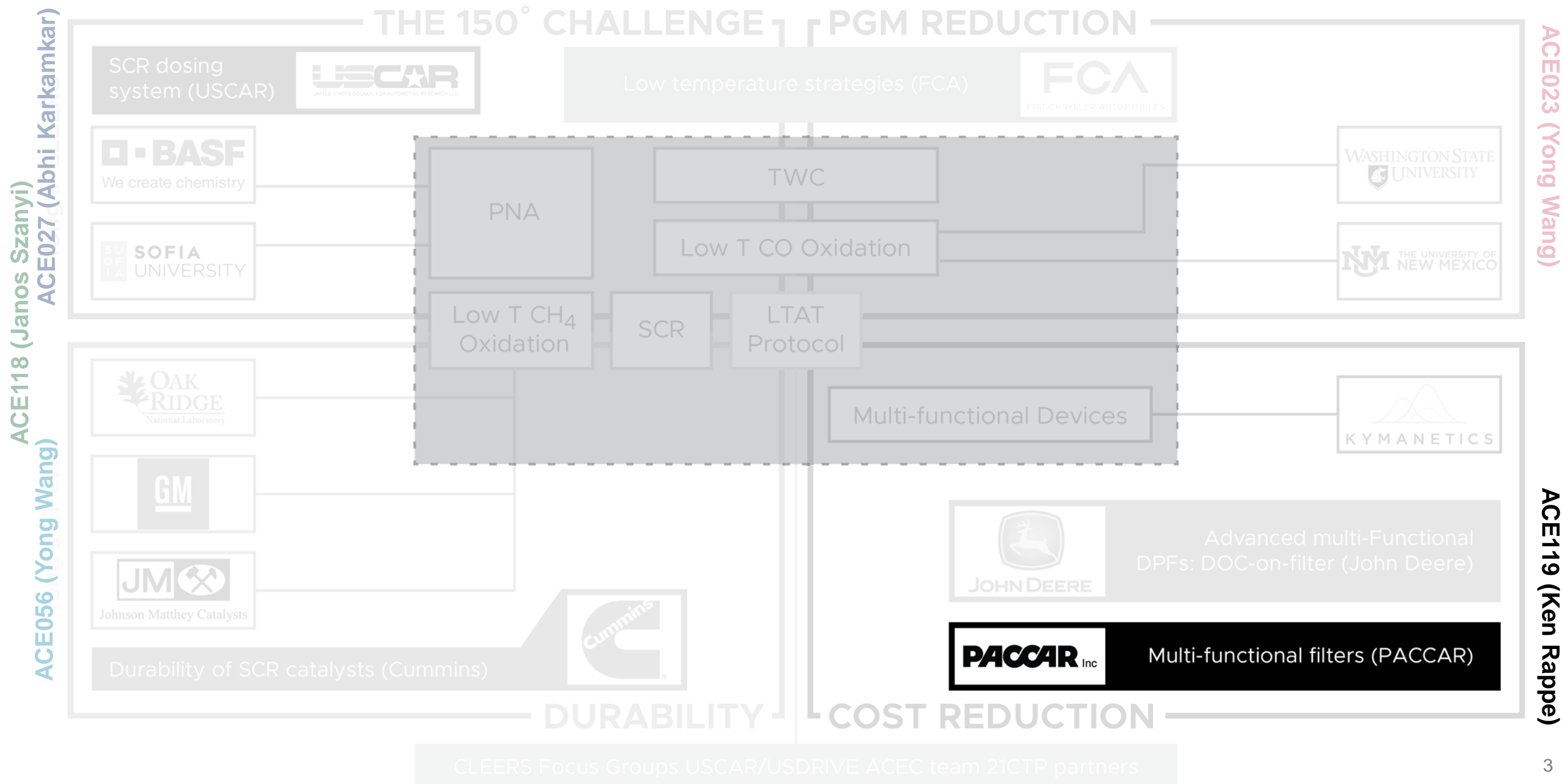
Feng Gao, Yong Wang



# PNNL Fundamental and CRADA Projects Address the 150°C Challenge, PGM Reduction, Durability, and Cost - Exemplified by 5 AMR Presentations



# PNNL Fundamental and CRADA Projects Address the 150°C Challenge, PGM Reduction, Durability, and Cost - Exemplified by 5 AMR Presentations



# Project Overview

## Timeline

- 4-yr CRADA
  - Start date – July 2016
  - End date – June 2020
- 95% complete

## Barriers

- **B. Lack of cost-effective emission control** for meeting EPA standards for NOx & PM emissions
- **E. Durability** of the emission control system: 435,000 miles (HD)
- **G. Cost of emission control** devices... for heavy duty engines in particular

## Budget

- Contract value – \$2.7M
  - \$1.35M DOE share
  - \$1.35M PACCAR share
- Funding received
  - \$1.1M through FY18
  - FY20 – \$100K

## Partners



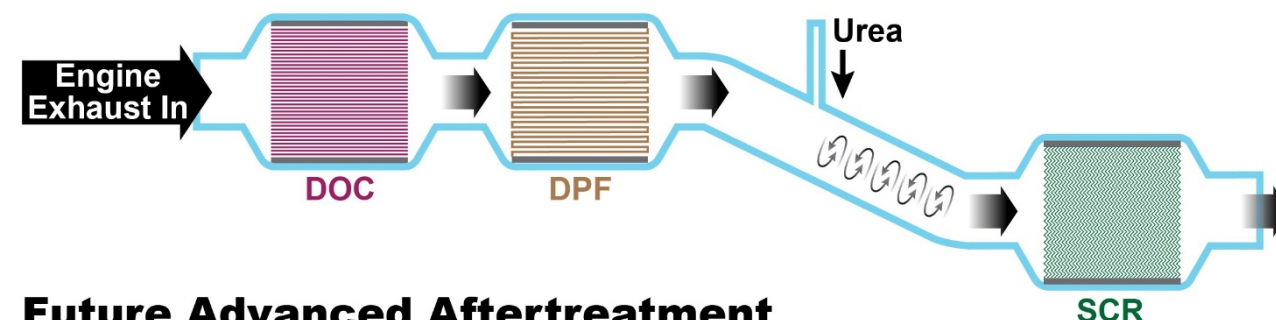
**PACCAR** Inc

- CRADA partner

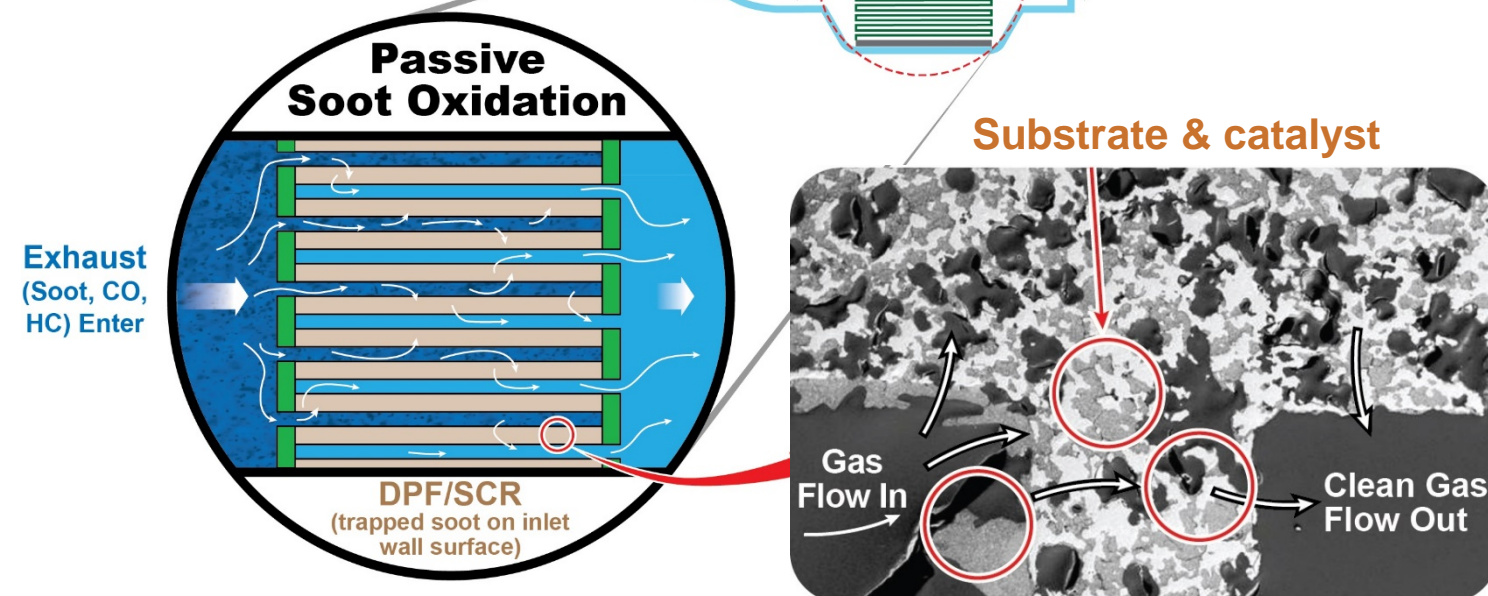
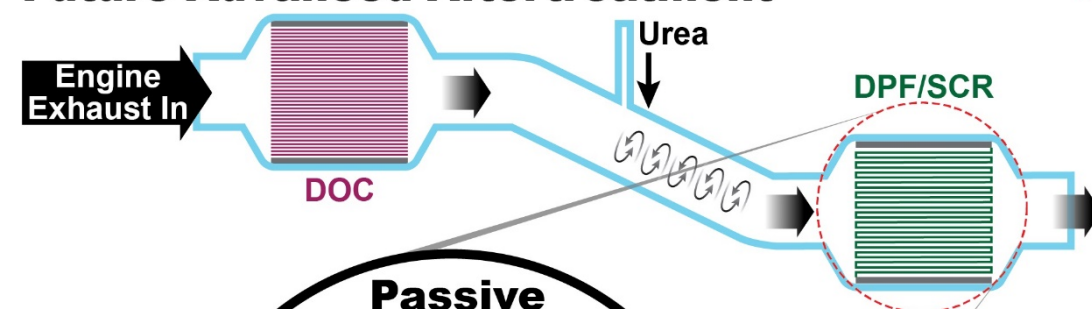


# Multi-Functional Aftertreatment: SCR-on-DPF for HD

## Current 2017 HD Aftertreatment



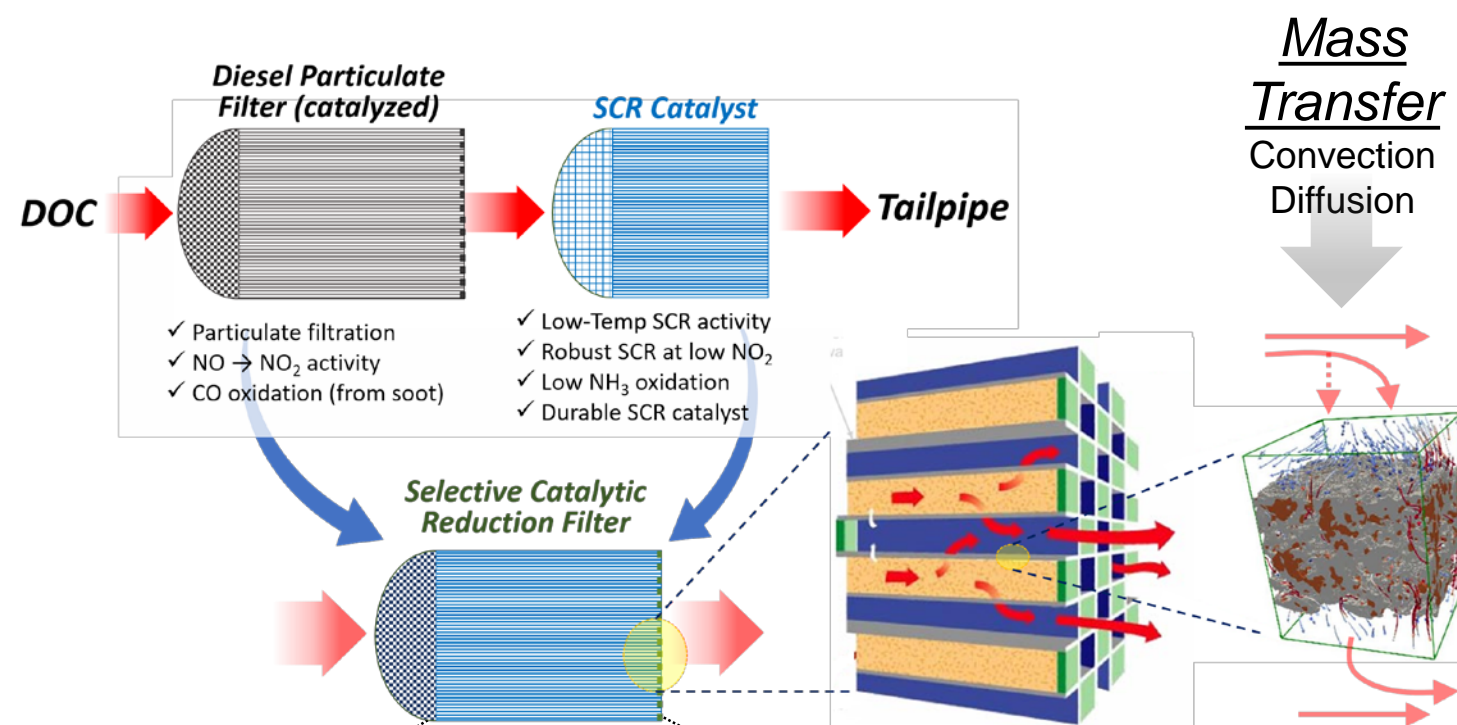
## Future Advanced Aftertreatment



- Highly promising strategy of aftertreatment integration
  - Reduced total thermal mass
    - ✓ Faster warm-up
    - ✓ Reduced cold-start emissions
  - Improved performance & increased flexibility
    - ✓ SCR more closely coupled to engine
    - ✓ Increased total SCR volume
- ✓ Soot trapped upstream
- ✓ Molecular diffusion to washcoat

## Relevance

# Fast SCR depletes $\text{NO}_2$ in inlet channel leaving less for passive soot oxidation

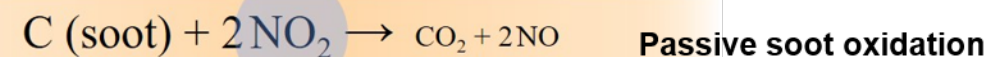
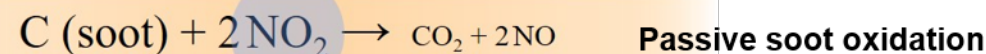
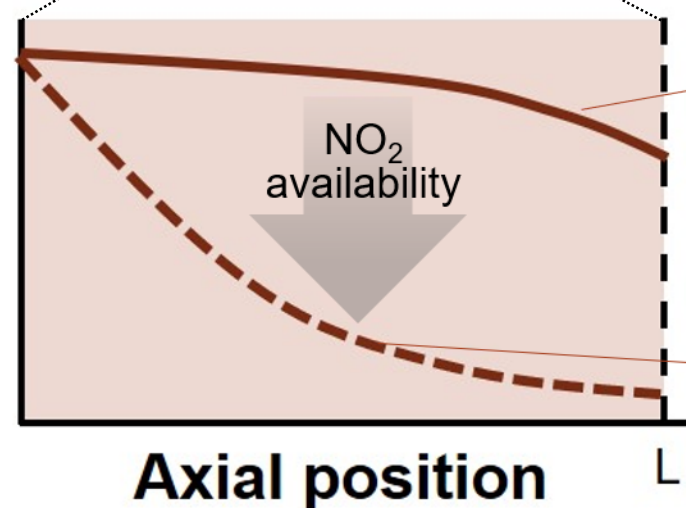


## Challenges to deployment

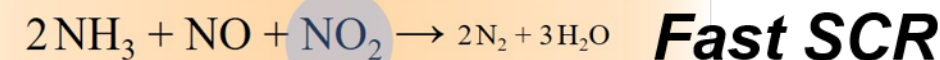
1. SCR performance (enough SCR)
2. SCR durability (extreme temps)

### 3. Passive soot oxidation

**$\text{NO}_2$  concentration  
in Inlet Channel**



+





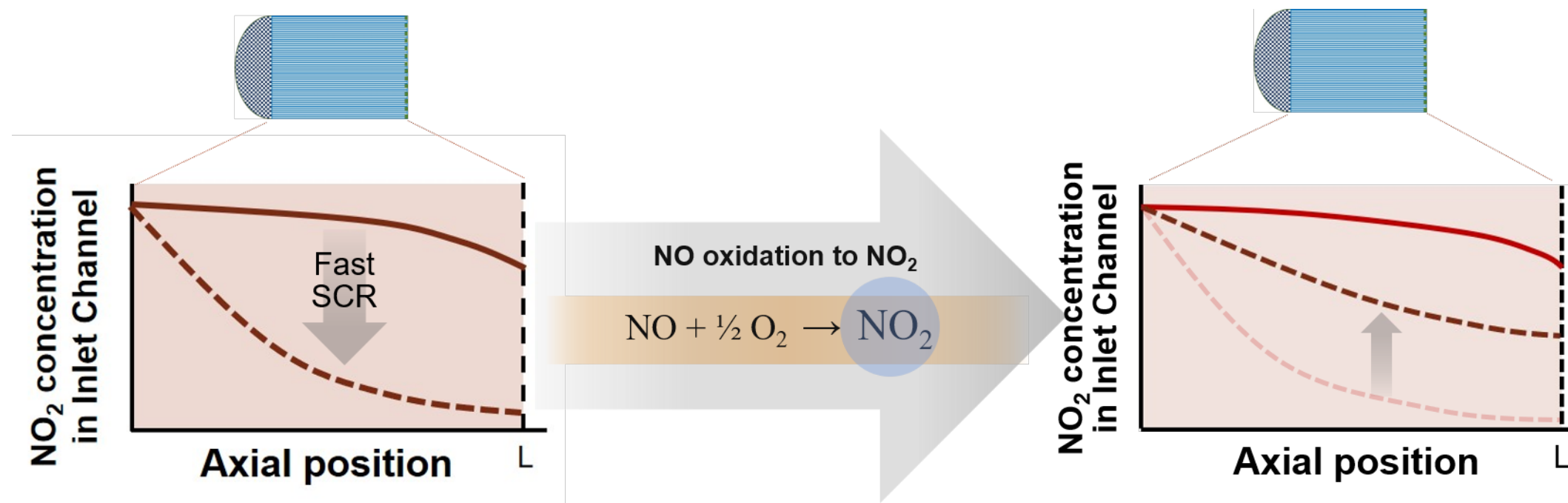
# The role of the SCO phase

Goal: Maximize passive soot oxidation activity with SCR on filter

Approach: Minimize the impact of fast-SCR catalysis on inlet  $\text{NO}_2$

***This is a catalysis challenge.***

- Use a selective catalytic oxidation (SCO) phase with the SCR catalyst to promote oxidation of NO to  $\text{NO}_2$
  - Increase  $\text{NO}_2$  in the filter inlet channel by ***reducing  $\text{NO}_2$  forward diffusive effects***
- Mn-based SCO phase being pursued



## Approach Schedule and Milestones

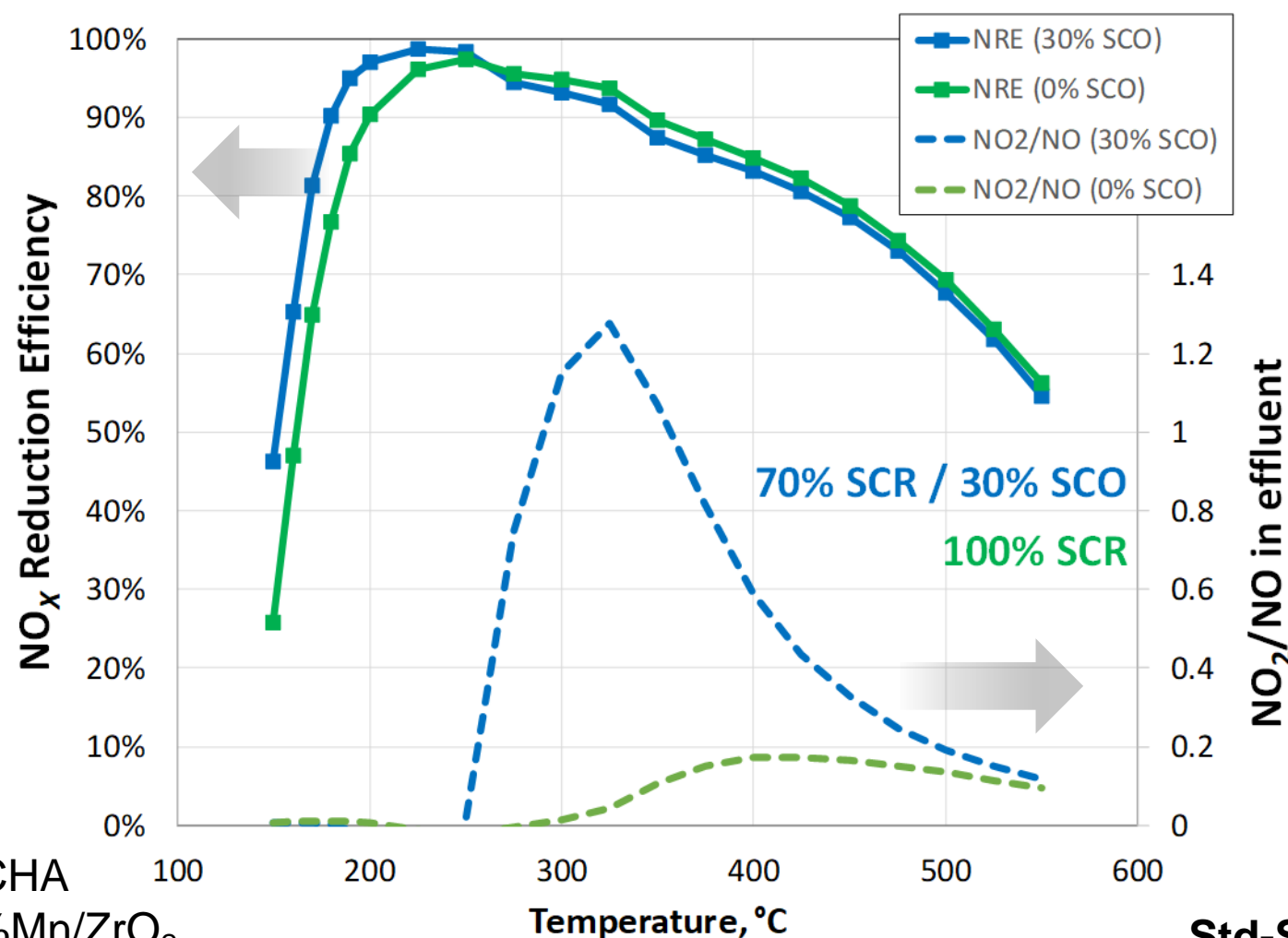
Date	Milestone and Go/No-Go Decisions	Status
May 2019	<u>Milestone:</u> SCRF single wall model complete	Complete
July 2019	<u>Go/No-Go decision:</u> SCO-SCR binary catalyst demonstrated that exhibits improved SCR/PSO performance and durability	Complete (PNNL + PACCAR)
Feb 2020	<u>SMART milestone:</u> SCRF binary catalyst development complete	Complete
April 2020	<u>Milestone:</u> SCRF device-level model complete	On-going



- Core sampling testing
  - SCR = CuCHA
  - SCO = 10%Mn/ZrO<sub>2</sub>
  - Most work is comparing
    - ✓ 100% SCR
    - ✓ 30% SCO – 70% SCR physically mixed (intimate)
- Axisuite modeling in progress
- SCO phase study and path forward

# SCO phase shown to significantly shift $\text{NO}_2/\text{NO}_x$ balance with equivalent or superior SCR performance

- Core sample testing – **Std SCR conditions**
- ~70 g/L active phase on SiC support



- Low temperature SCR activity improvement
- No adverse impact of  $\text{NH}_3$  oxidation at elevated temperature
- Significantly increased  $\text{NO}_2$  in catalyst effluent
  - 290°C to 360°C

↓

$\text{NO}_2 > \text{NO}$  in effluent

SCR = CuCHA  
SCO = 10%Mn/ZrO<sub>2</sub>

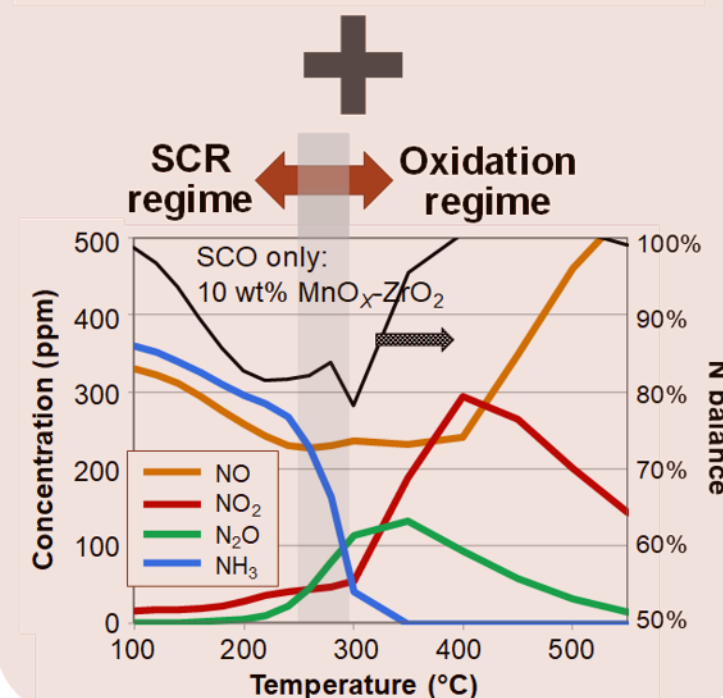
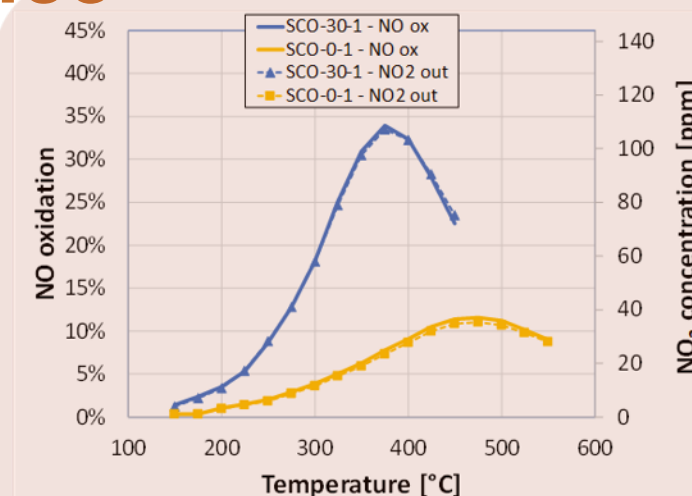
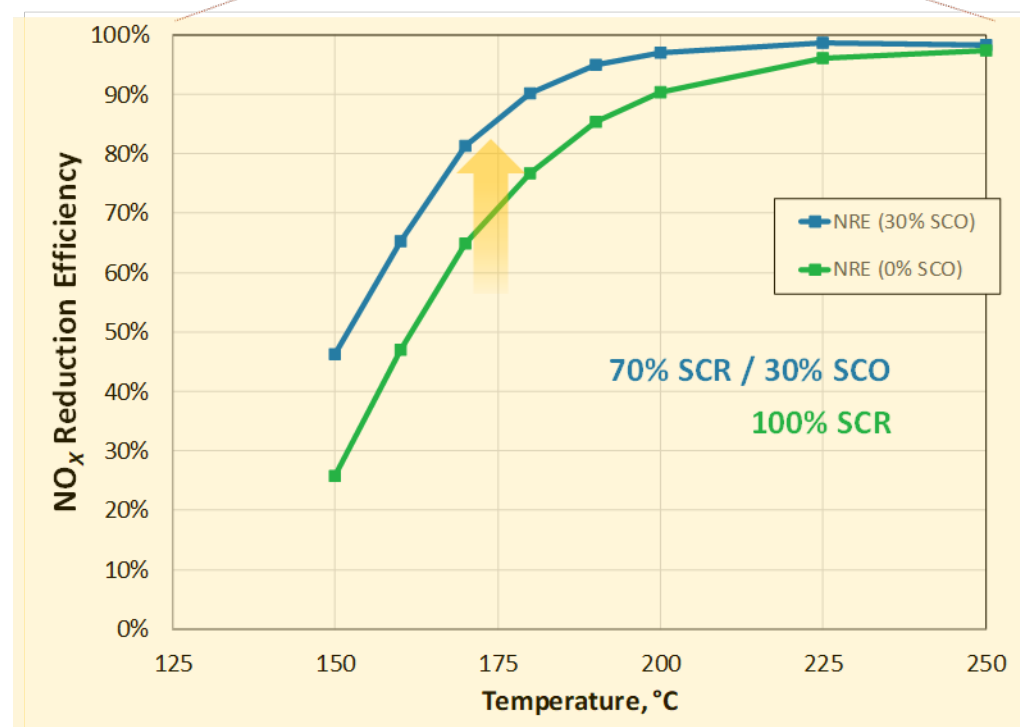
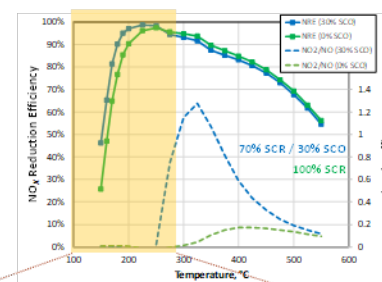
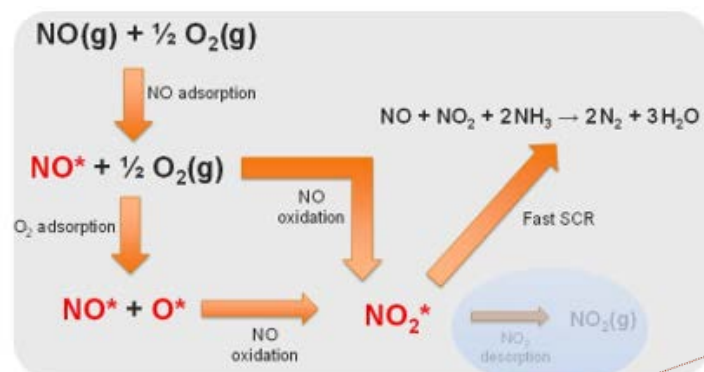
## Std-SCR Conditions:

300 ppm NO, 10% O<sub>2</sub>, 6% H<sub>2</sub>O, Balance N<sub>2</sub>, SV=35K/hr <sup>10</sup>



## Accomplishments

# SCO-SCR synergistic interaction observed from superior low-temperature SCR performance



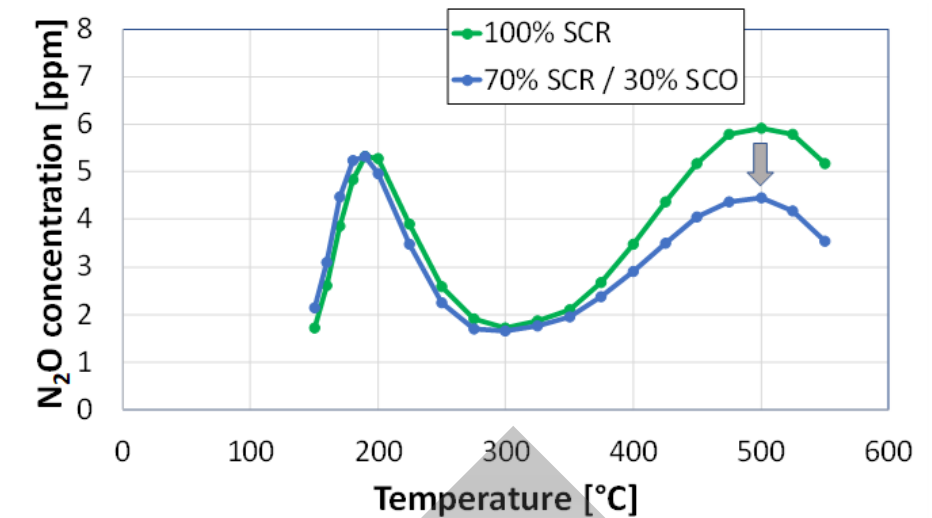
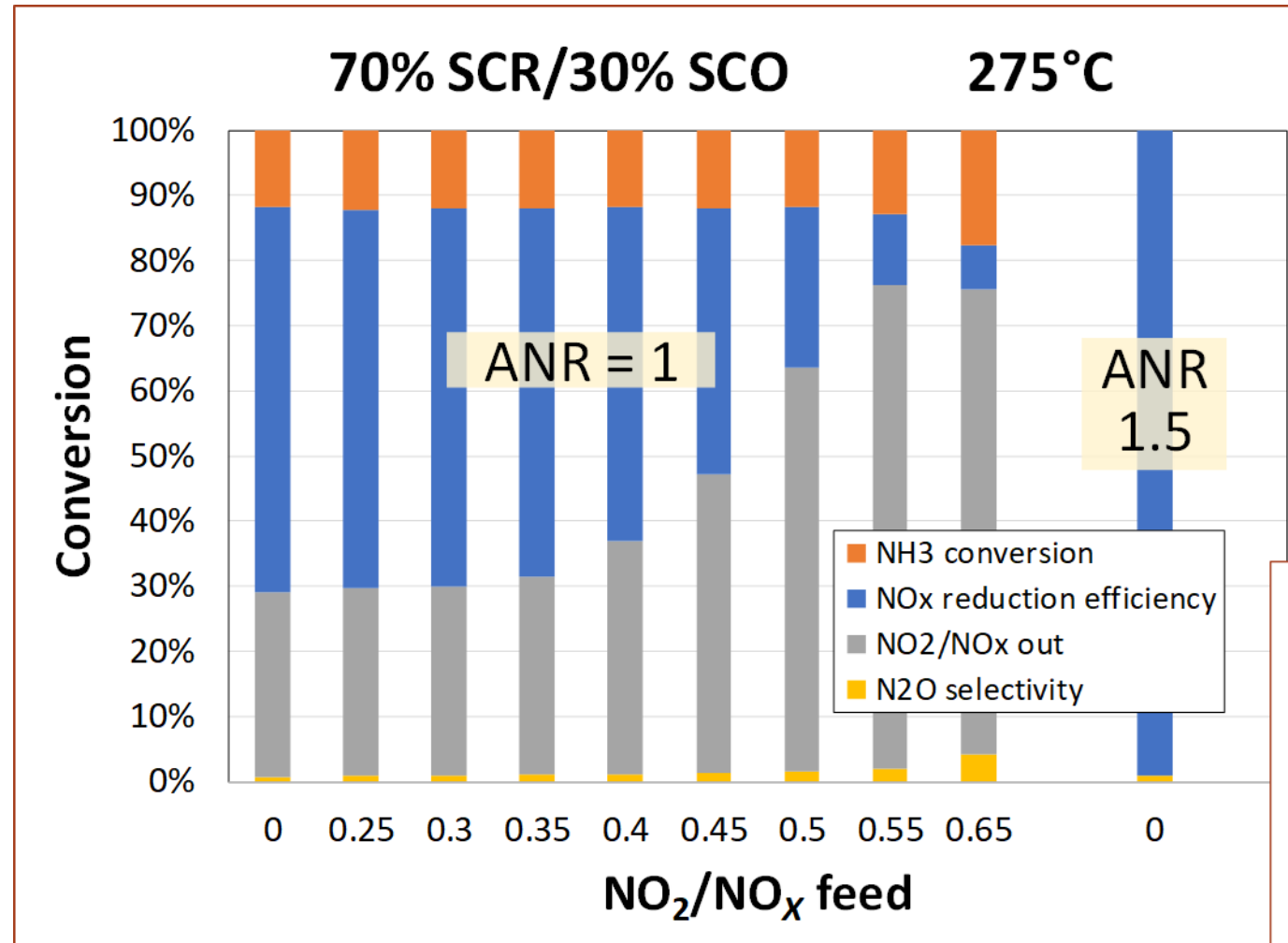
Low-temperature SCR performance improvement from binary catalyst



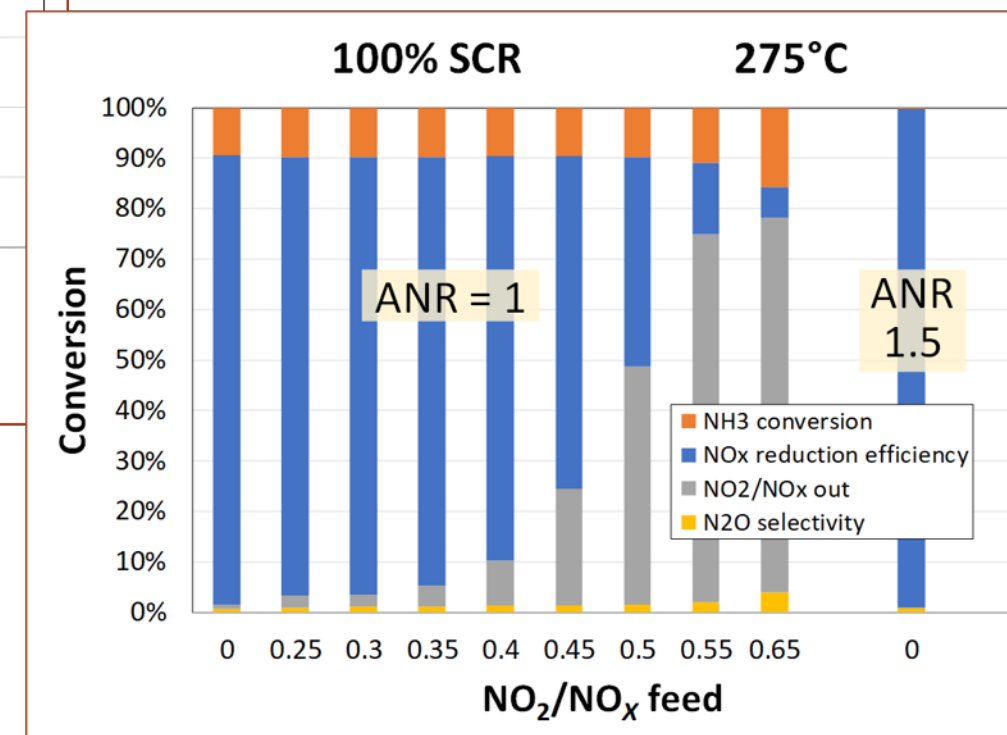
NO oxidation + SCO-phase SCR contribution

## Accomplishments

# SCO phase exhibits durable impact on $\text{NO}_2/\text{NO}_x$ balance across all expected gas compositions



Analogous or improved  
N<sub>2</sub>O effluent profile!



SCO contribution has durable impact across broad NO/NO<sub>2</sub> make-up



## Approach

# Soot oxidation testing procedure

Soot loading & soot oxidation  
are decoupled and performed  
iteratively

2.76 kg/min 35K GHSV

300 ppm NO<sub>x</sub> & NH<sub>3</sub>  
10% O<sub>2</sub>, 6% H<sub>2</sub>O



## Sequence

- Load to ~4 g/L soot loading on real soot generator unit
- Remove from soot generator apparatus, install into synthetic gas bench
- Pre-heat and stabilize inlet gas profile
- Temperature programmed oxidation @ 5°C/min 150°C (or 180°C) to 580°C

## Metrics

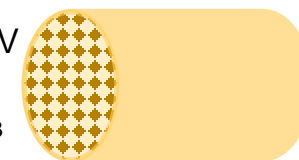
- Pressure drop
- CO, CO<sub>2</sub> production
  - Soot mass is not reliable on mini-cores

## Accomplishments

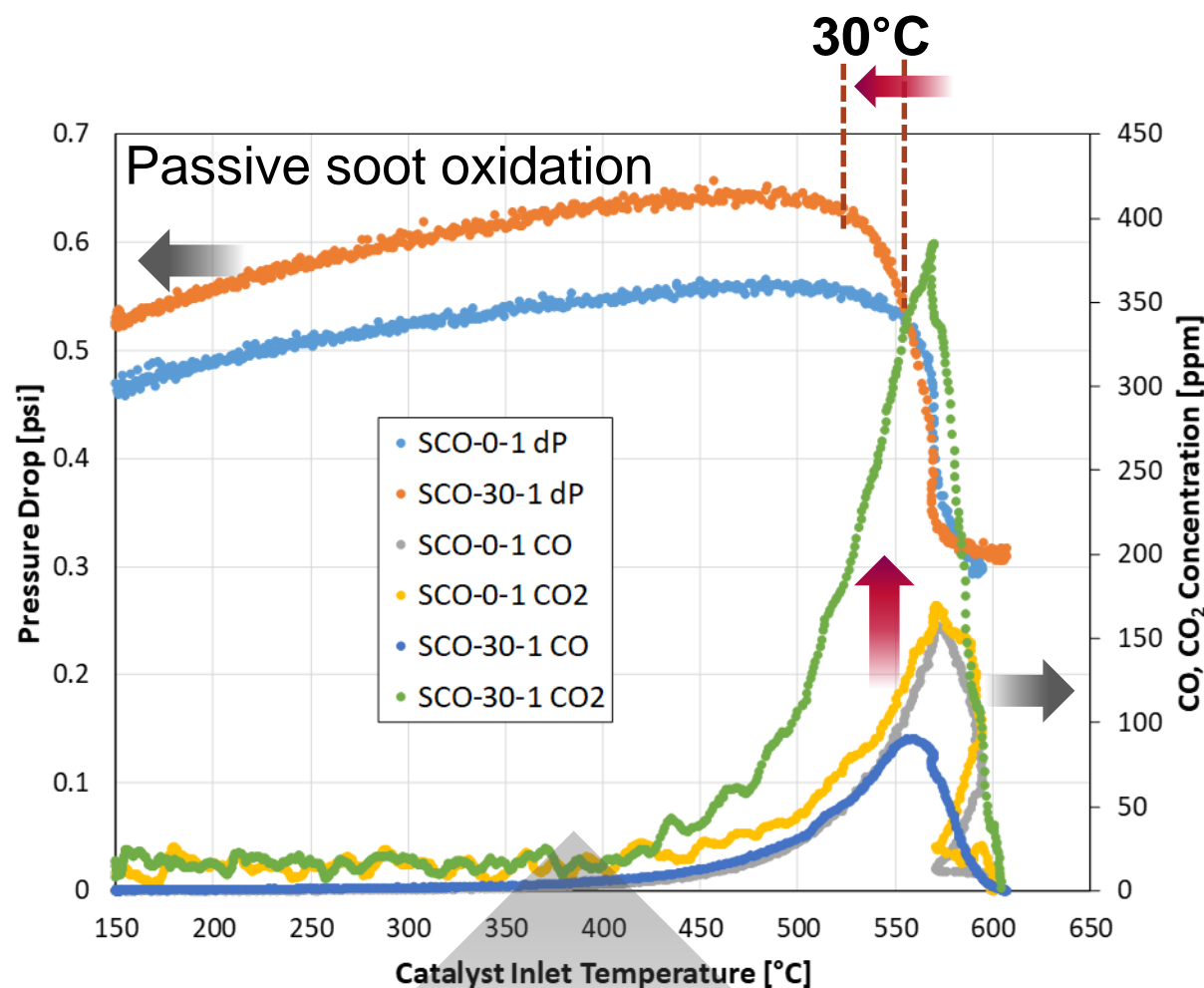
# SCO phase positively impacts passive soot oxidation activity and CO/CO<sub>2</sub> production profile

2.76 kg/min 35K GHSV

300 ppm NO<sub>x</sub> & NH<sub>3</sub>  
10% O<sub>2</sub>, 6% H<sub>2</sub>O

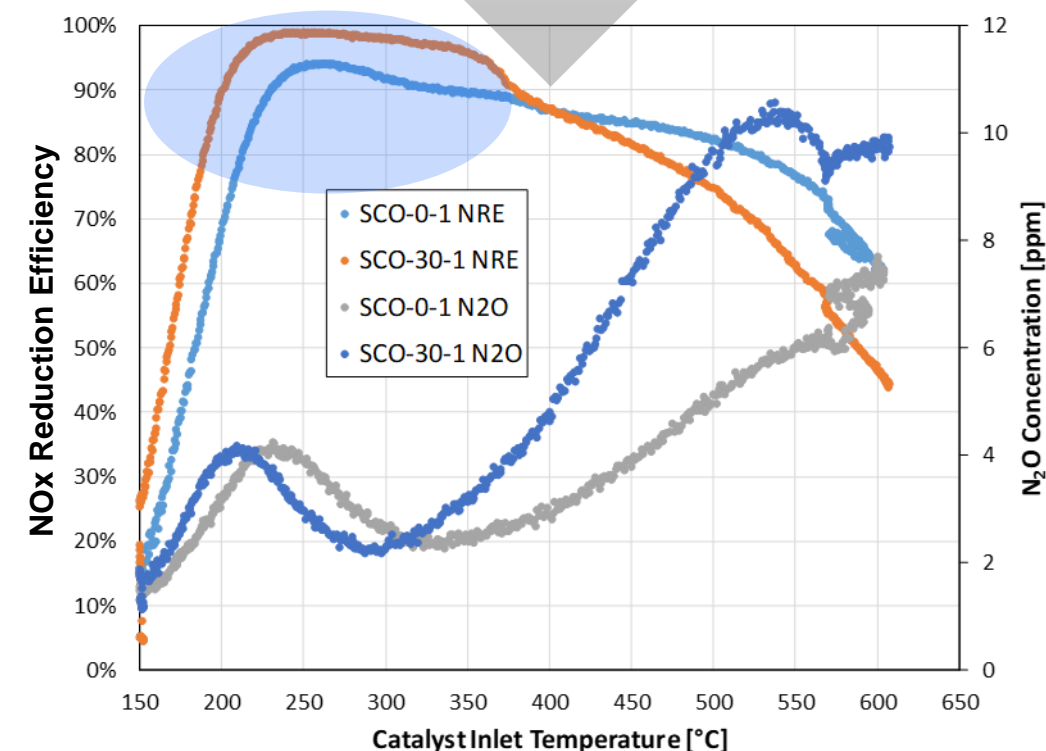


**Std-SCR Conditions**



- SCO shifts pressure drop profile to ~30°C lower
- Effluent shifted to CO<sub>2</sub> majority (versus CO production) \*\*

- SCO benefits std-SCR through >350°C

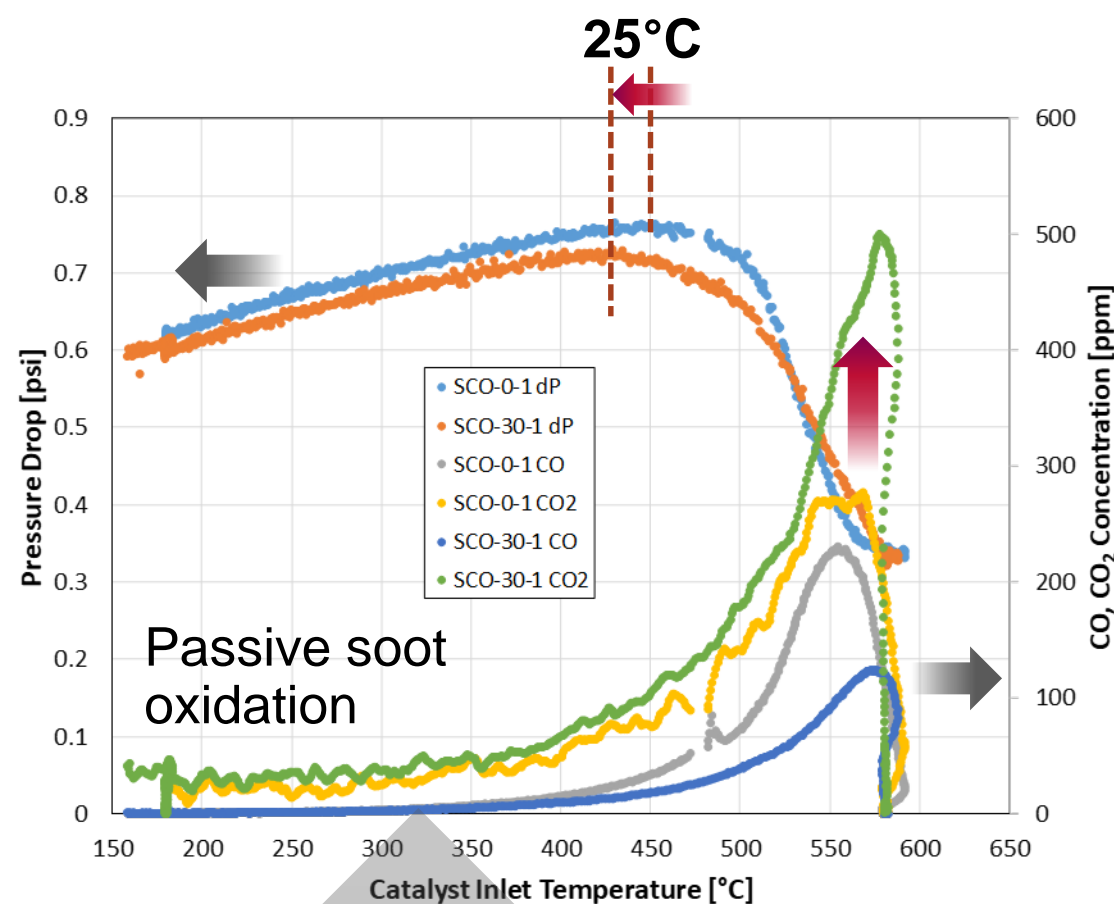


\*\*Important because filter will not have PGM-based CO oxidation



## Accomplishments

# With greater $\text{NO}_2$ in feed, soot oxidation $\text{CO}/\text{CO}_2$ product profile becomes main benefit of SCO phase

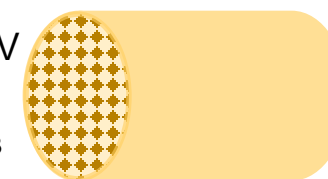


- $\text{NO}_2/\text{NO}_x = 0.35$
- $\Delta P$  profile to  $\sim 30^\circ\text{C}$  lower temperature
- Effluent *heavily* shifted to  $\text{CO}_2$  majority\*\*

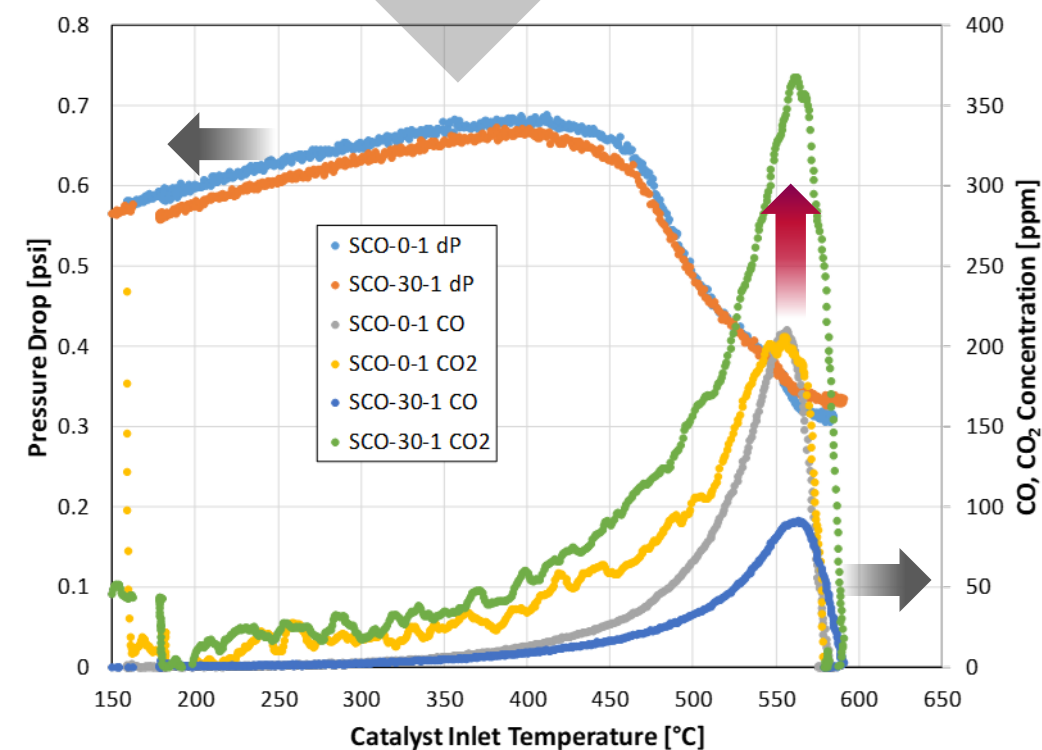
\*\*Important because filter will not have PGM-based CO oxidation

2.76 kg/min 35K GHSV

300 ppm  $\text{NO}_x$  &  $\text{NH}_3$   
10%  $\text{O}_2$ , 6%  $\text{H}_2\text{O}$

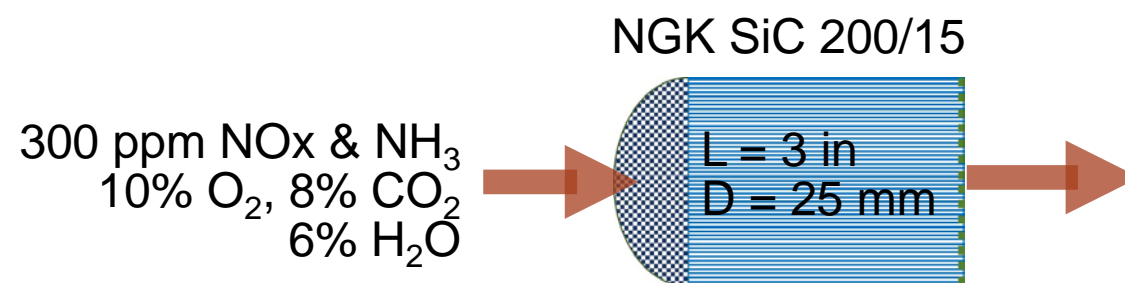


- $\text{NO}_2/\text{NO}_x = 0.5$
- Effluent *heavily* shifted to  $\text{CO}_2$  majority\*\*



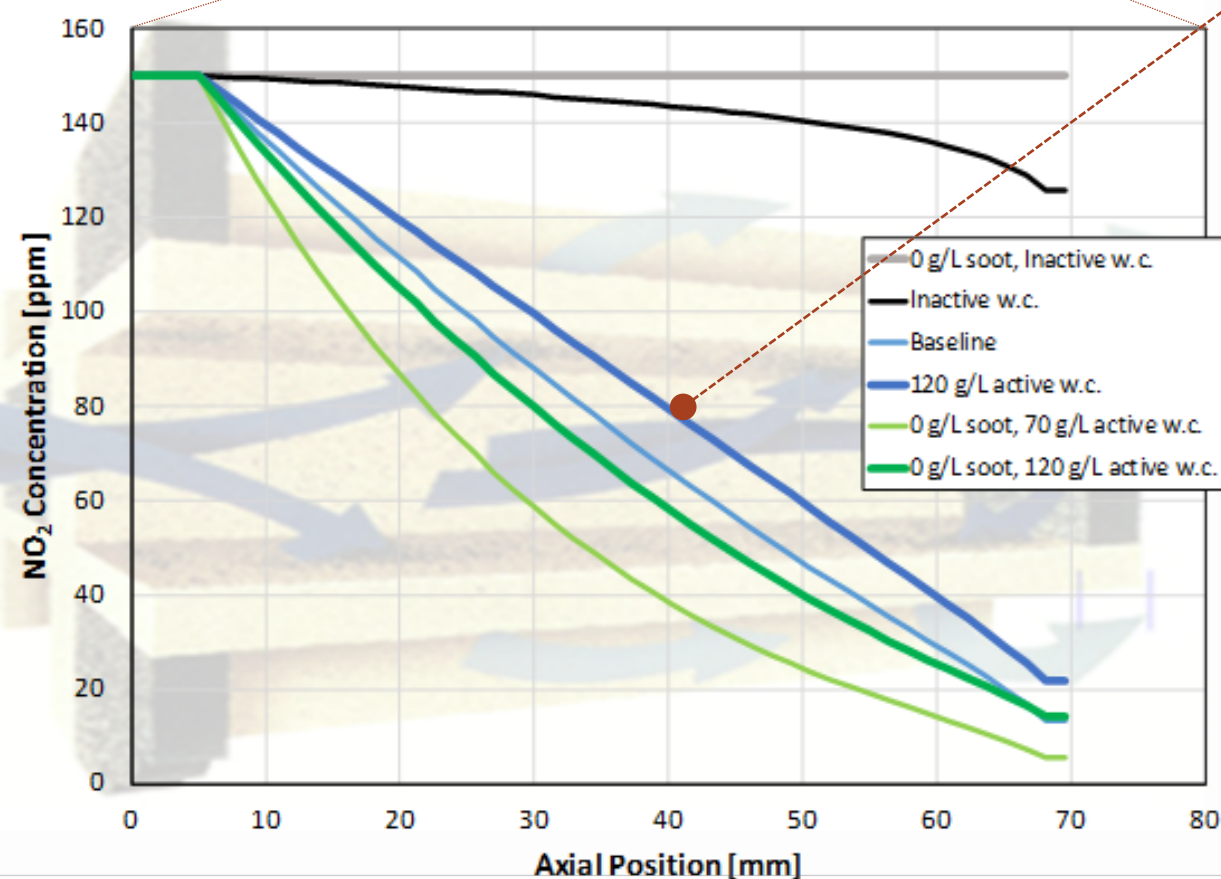
## Accomplishments

# Axisuite modeling shows the pronounced impact that wall velocity has on diffusive impacts



Great SCR catalyst increases [NO<sub>2</sub>] in inlet channel

- Increases wall flow velocity
- Decreases diffusion contribution



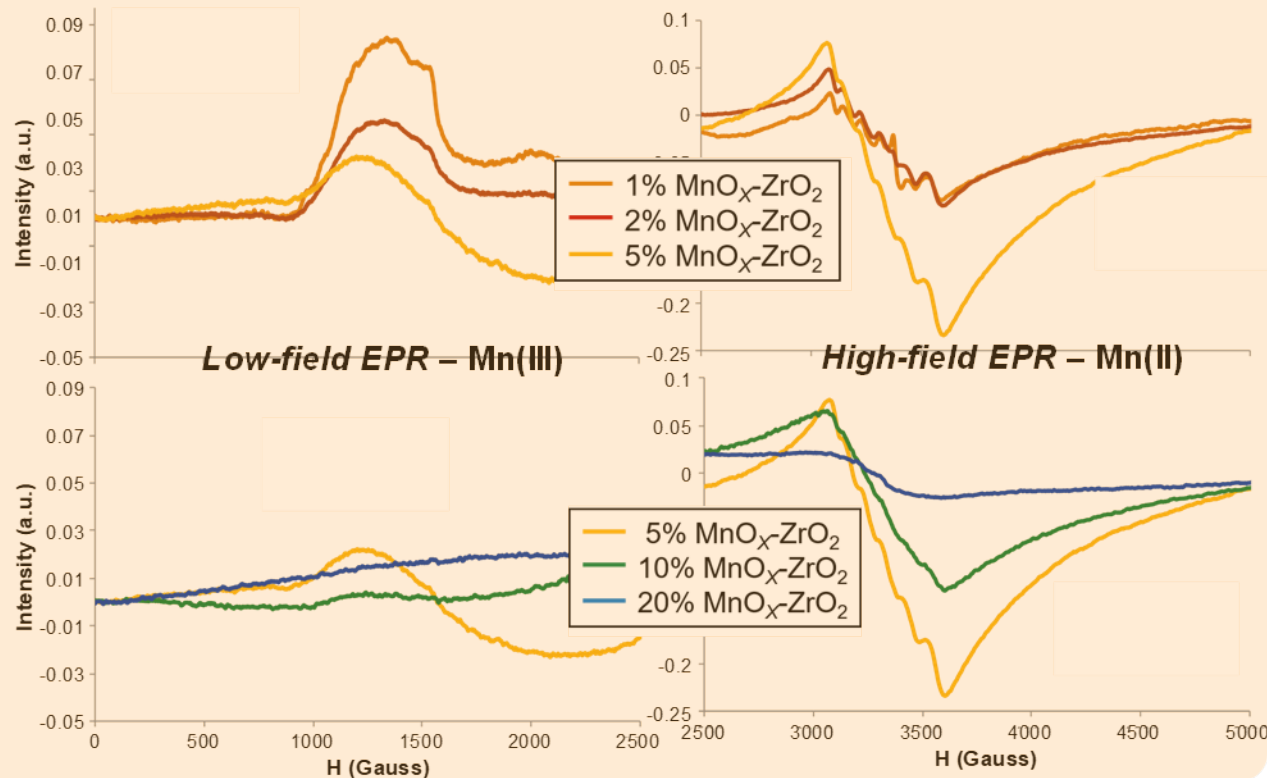
- 250°C
- Baseline: 35K GHSV, 4 g/L soot, 70 g/L active w/c distribution = 1

Simulating bench-scale testing of catalyst cores



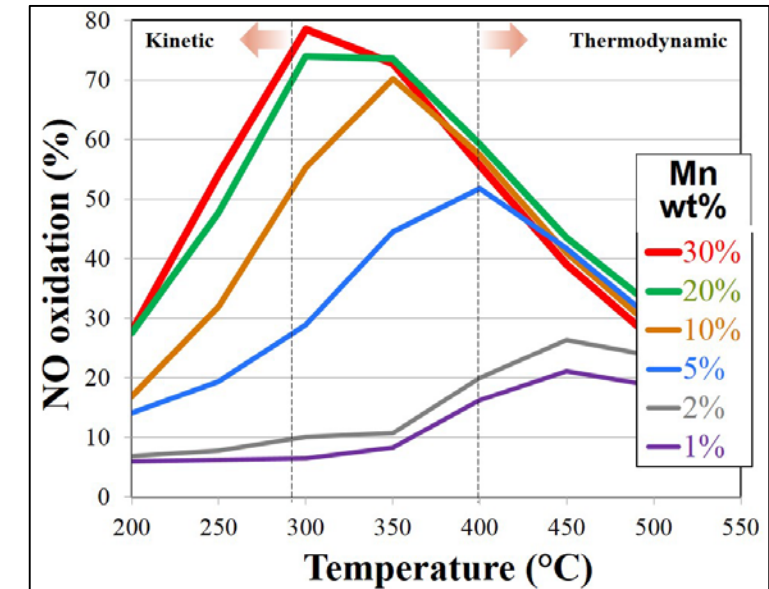
# Mn-dimer active center, directs pathways for improved thermal and chemical durability

<5% Mn:  $\uparrow$  Mn =  $\uparrow$  Mn(II) &  $\downarrow$  Mn(III) proportionally

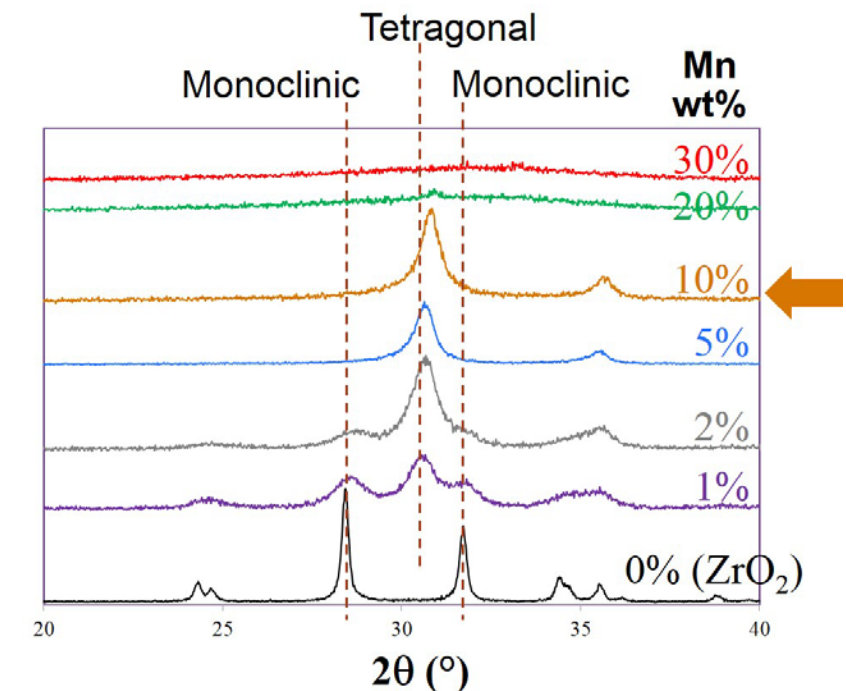


>5% Mn:  $\uparrow$  Mn =  $\downarrow$  Mn(II) &  $\downarrow$  Mn(III) proportionally

- Shift to non-isolated Mn species at 5 wt%
- Optimum NO oxidation at 10 wt% Mn,
- Suggests Mn-dimer active center



**10 wt% MnO<sub>2</sub> optimum loading on ZrO<sub>2</sub> for catalyst development**

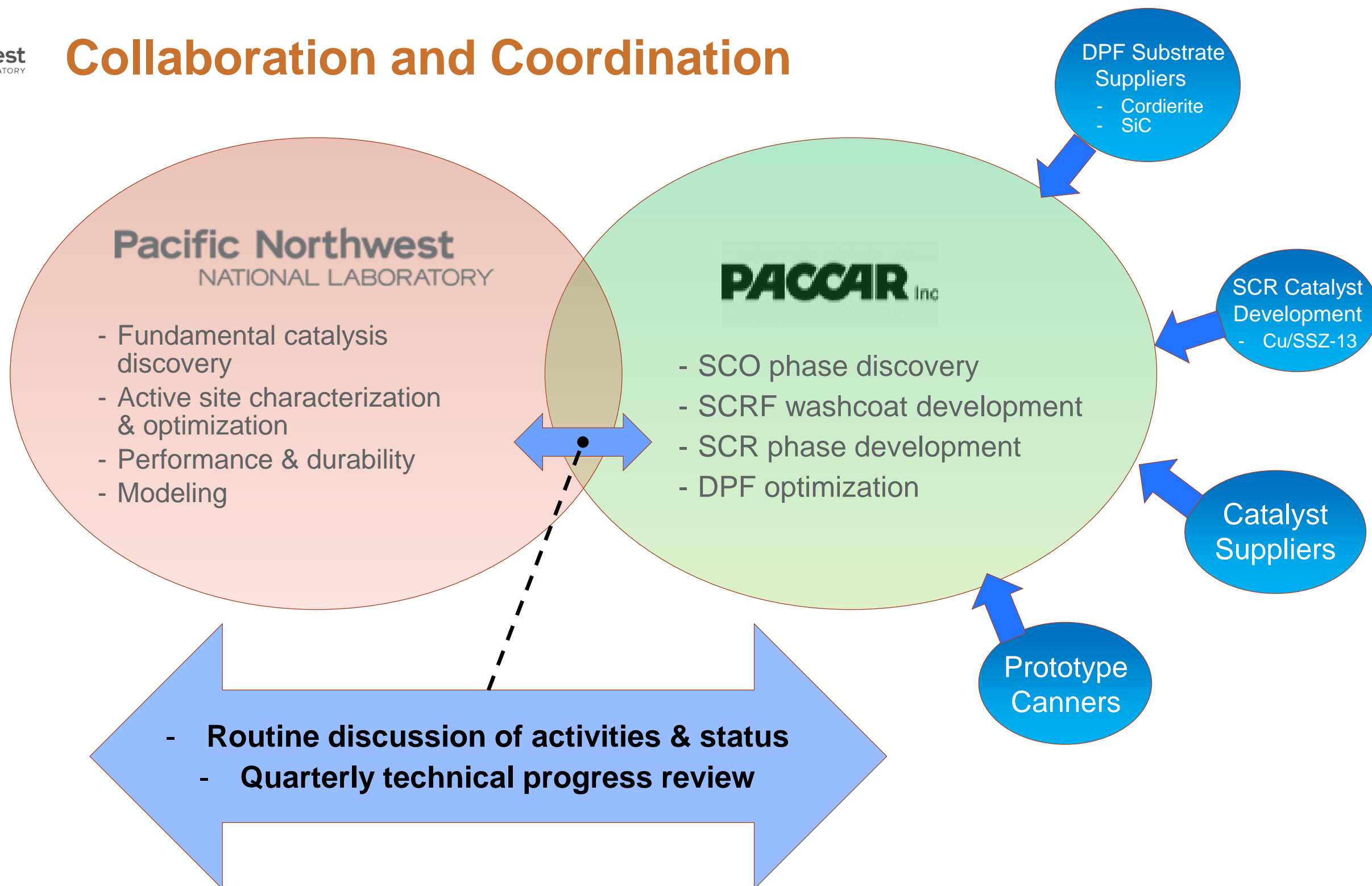


# Responses to Reviewer Comments

Comment	Response
Thermal/chemical aging needs to be addressed; GHG emissions (N <sub>2</sub> O, CH <sub>4</sub> ) should be addressed as well	<p><u>Reviewer is correct!</u> Thermal aging has been an area of focus for the work. Last year, showed unique thermally-induced IE aging mechanism (Mn displacing Cu) and relevance to heavy-duty diesel application.</p> <p>N<sub>2</sub>O emission profile shown this year.</p> <p>This year sulfur is an area of focus; work is proceeding.</p>
Unclear if “newer” NO <sub>2</sub> formed <i>in-situ</i> is not consumed by NH <sub>3</sub> .	<p>We can measure it. We are able to track the fate of NH<sub>3</sub> to routes <i>other</i> than SCR, e.g., oxidation by CuO clusters. We call this ‘parasitic’ NH<sub>3</sub> oxidation.</p>
Modest outcome compared to current state-of-the-art which is in industry for >10 years	<p>Yes, SCR-on-DPF is available technology for <u>light-duty</u>, enabled by durable CuCHA and high-porosity filter substrates. Not the case for <u>heavy-duty</u>. Current technology prohibitively impacts passive soot oxidation and increases aftertreatment fuel penalty.</p>



# Collaboration and Coordination



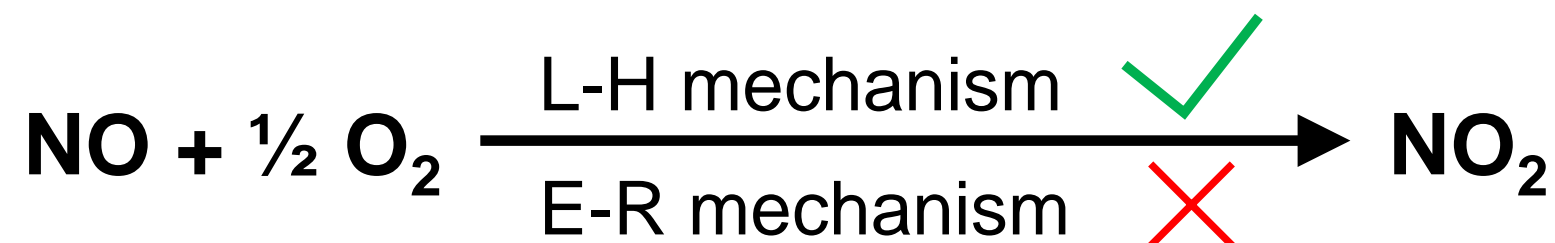
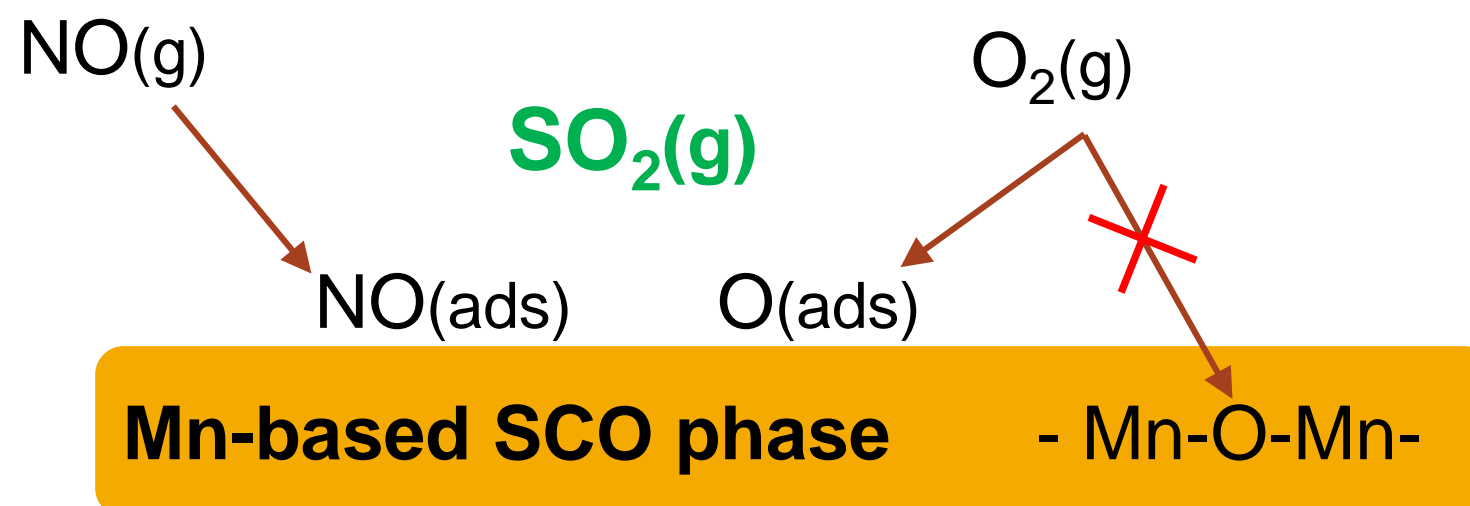
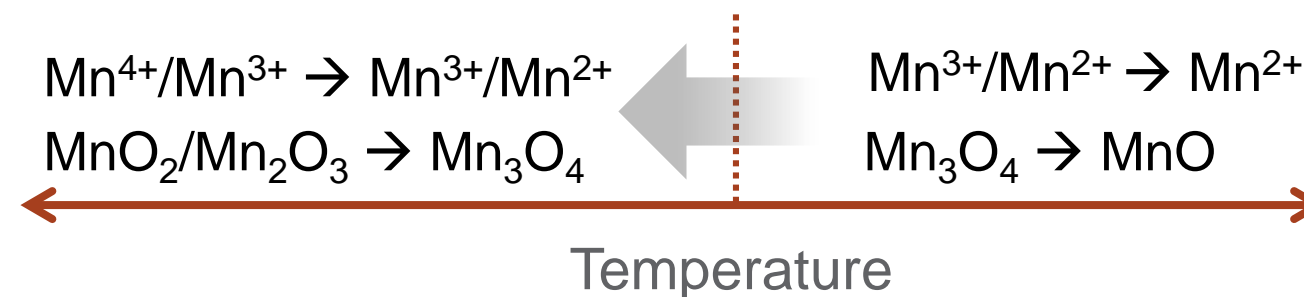
## Remaining Challenges

- Modeling – Accurately capturing all kinetic pathways of SCO-phase contribution.
  - NO oxidation, STD SCR, FAST SCR, NH<sub>3</sub> oxidation
  - Synergistic effect: how do we capture this?
- Chemical poisoning – MnO<sub>x</sub>/ZrO<sub>2</sub> solid solution, pursue pathways to address prohibitive interaction if present.



# Sulfur durability an area of focus for balance of program

Evidence suggests low-temperature reducibility of Mn may be key to sulfur resistant SCO phase through L-H reaction pathway



## Proposed Future Research

- Model development with full SCO kinetics
- Road-mapping studies with model
- Sulfur durability – SCO-phase modifications for improved reducibility
- Desulfation requirements as  $f(\text{reducibility})$



## Summary

- 10%Mn/ZrO<sub>2</sub> SCO phase shown to significantly shift NO<sub>2</sub>/NO<sub>x</sub> balance in the device with equivalent or superior SCR performance.
  - Durable impact on NO<sub>2</sub>/NO<sub>x</sub> balance across all expected gas compositions
- SCO-SCR synergistic interaction observed from superior low-temperature SCR performance not accounted for by [NO oxidation + SCO-phase SCR]
- SCO phase positively impacts passive soot oxidation activity and CO/CO<sub>2</sub> production profile
  - With greater NO<sub>2</sub> in feed, CO/CO<sub>2</sub> product profile becomes main benefit of SCO phase
- Axisuite modeling shows the pronounced impact that wall velocity has on diffusive impacts.
- Mn-dimer active center identified, directs pathways for improved thermal and chemical durability





**Pacific  
Northwest**  
NATIONAL LABORATORY

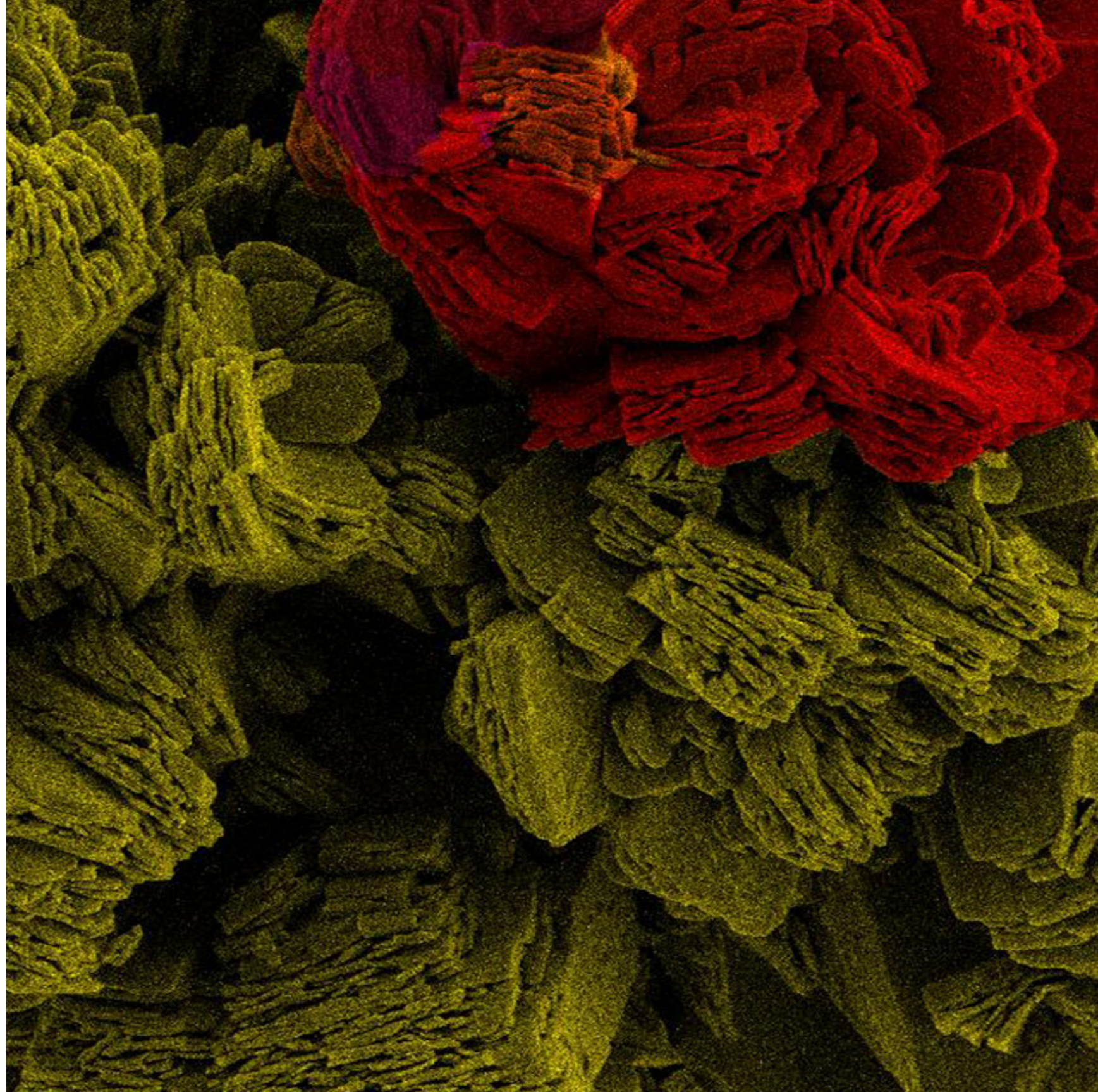
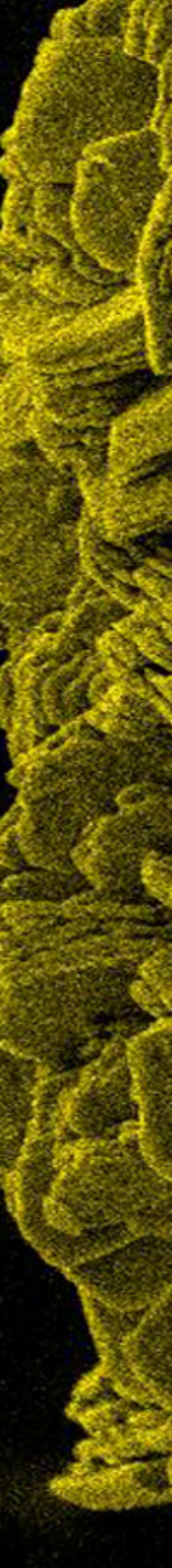
Institute for  
**INTEGRATED  
CATALYSIS**

# Thank you





## Back-up Slides



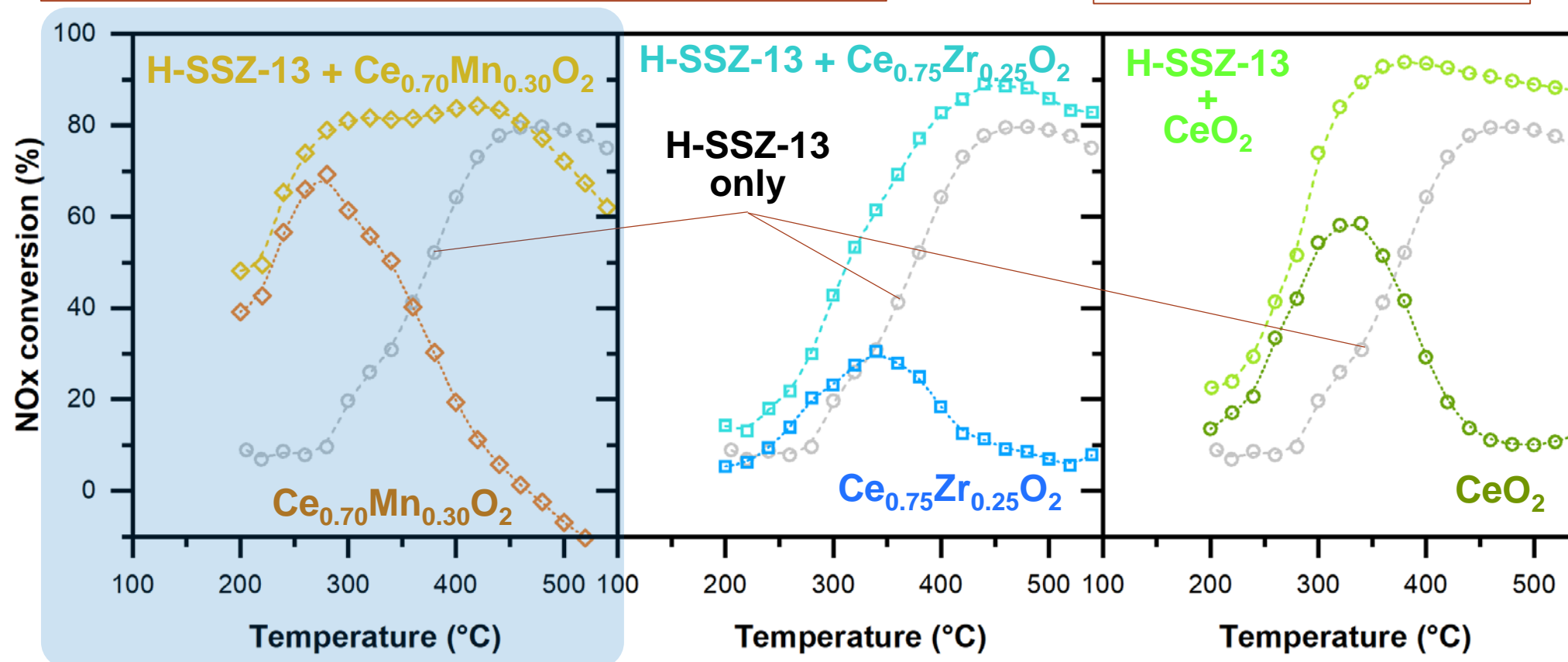


# Mn-based SCO showing greatest opportunity for synergistic low-temperature SCR impact

## Fast SCR

Fast SCR: 175 ppm NO, 175 ppm NO<sub>2</sub>, 350 ppm NH<sub>3</sub>, 15% O<sub>2</sub>, 6% H<sub>2</sub>O and 8% CO<sub>2</sub> (balanced N<sub>2</sub>), heating ramp of 2 °C min<sup>-1</sup>

150 mg catalyst,  
SV = 400 L g<sup>-1</sup> h<sup>-1</sup> (1000 sccm)

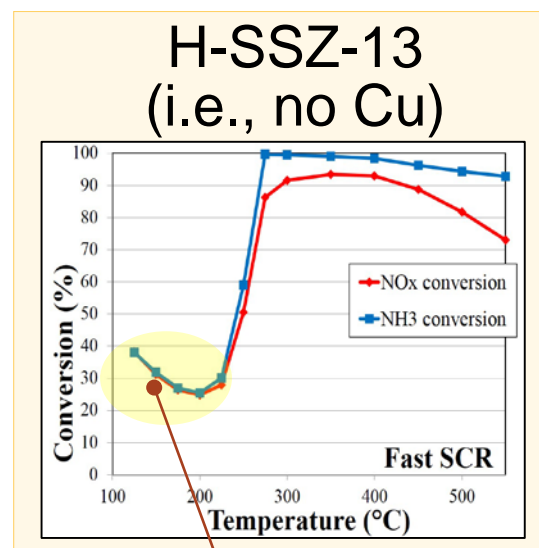


- 10% metal oxide phases co-impregnated onto H-form SSZ-13.
- H-form SSZ-13 (i.e., without Cu) used to highlight NO<sub>2</sub>–driven reaction pathways facilitated by the SCO phase.
- Data highlights NO<sub>2</sub> SCR reaction pathways facilitated by SCO phase.

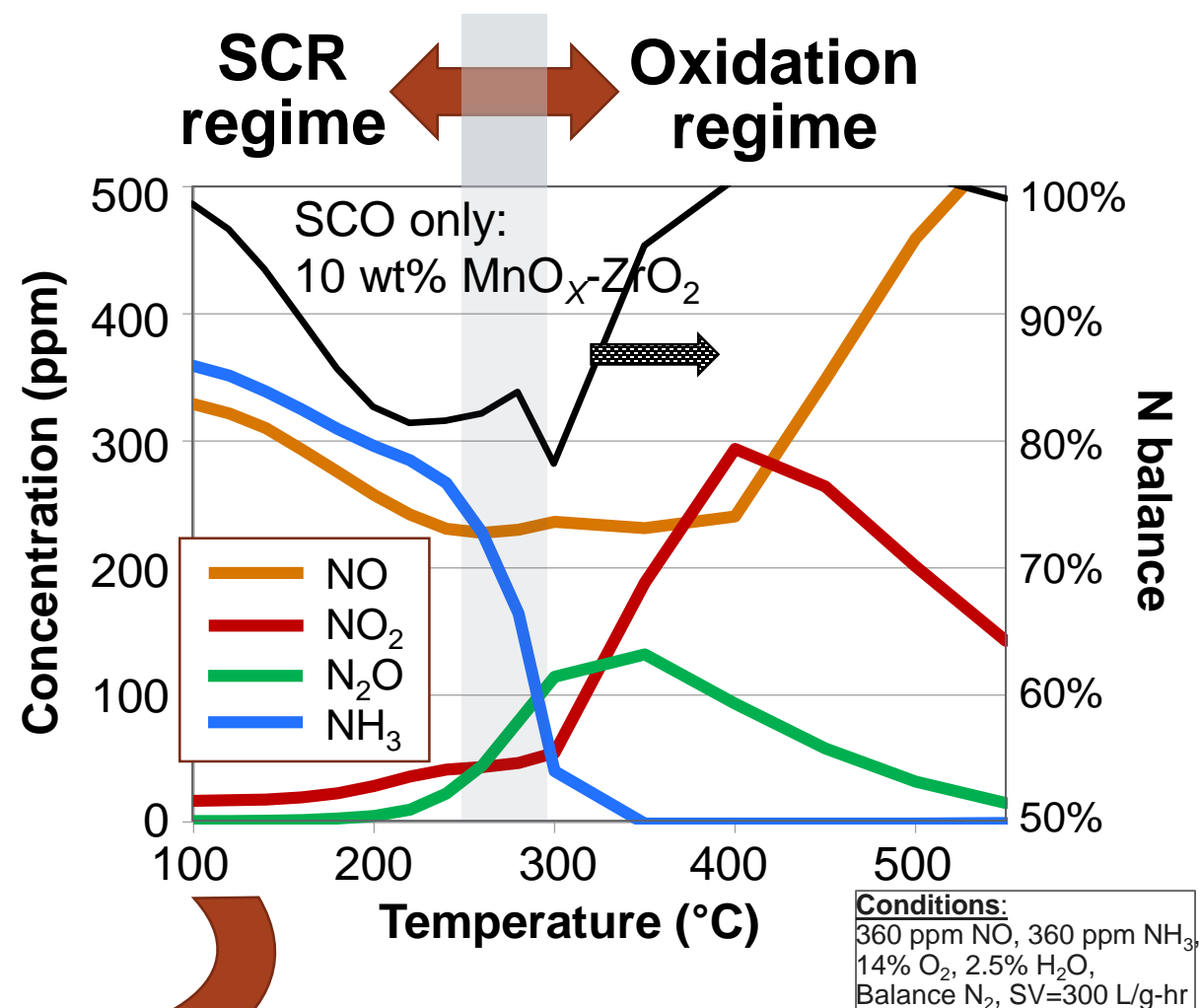
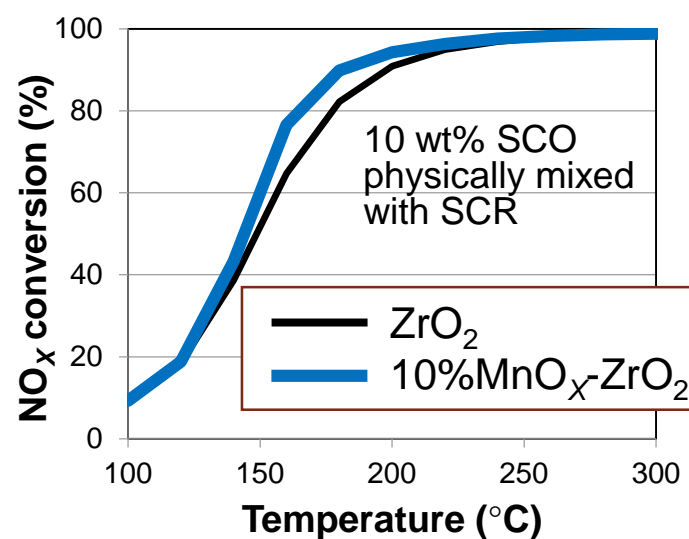


## Accomplishments

# SCO phase shown to have bi-functionality demonstrating both SCR and oxidation regimes



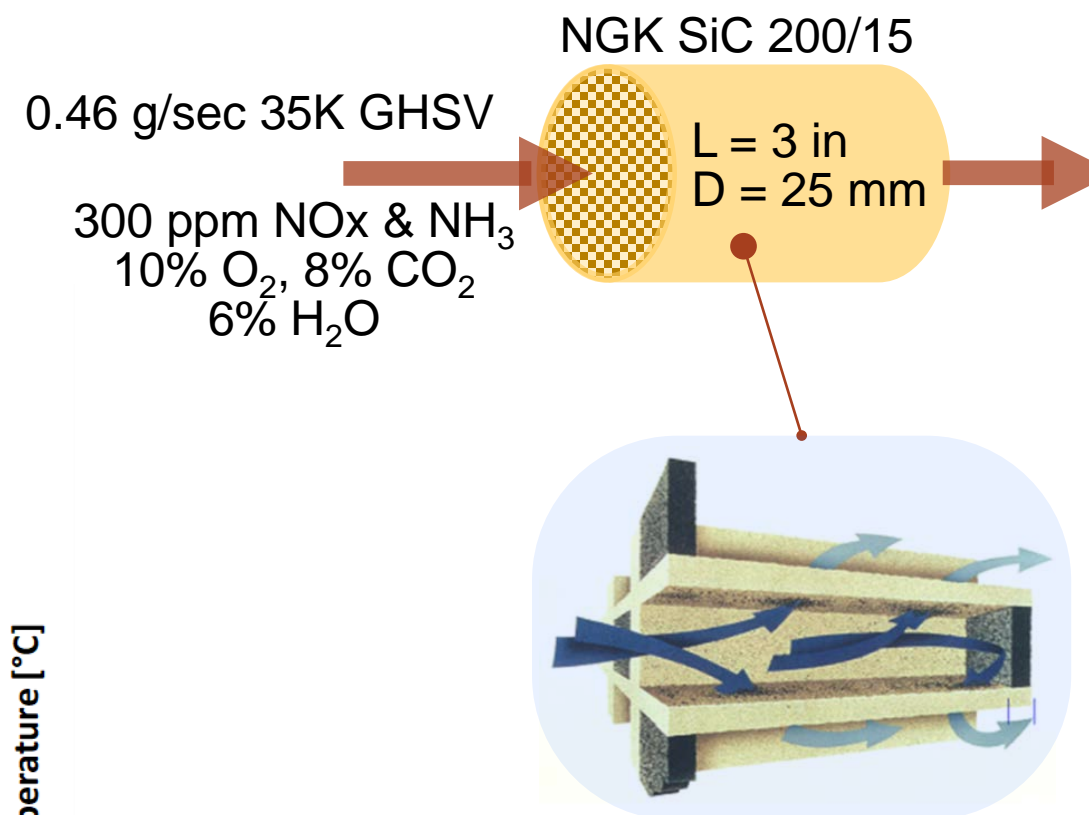
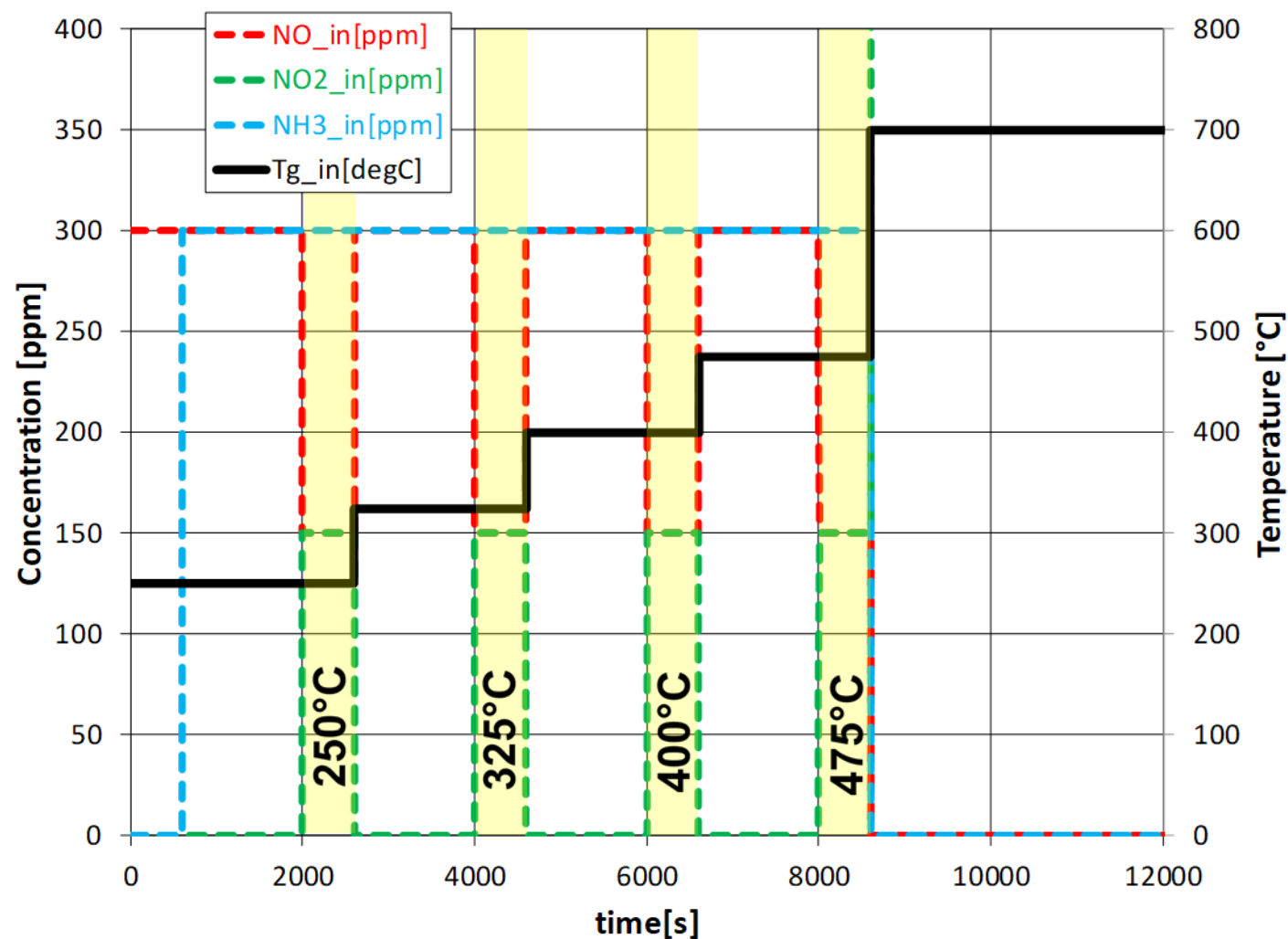
Not promoted  
Nitrate formation



SCO phase exhibits low-temperature SCR while promoting higher temperature oxidation function

# Axisuite modeling structure built to match bench reactor data

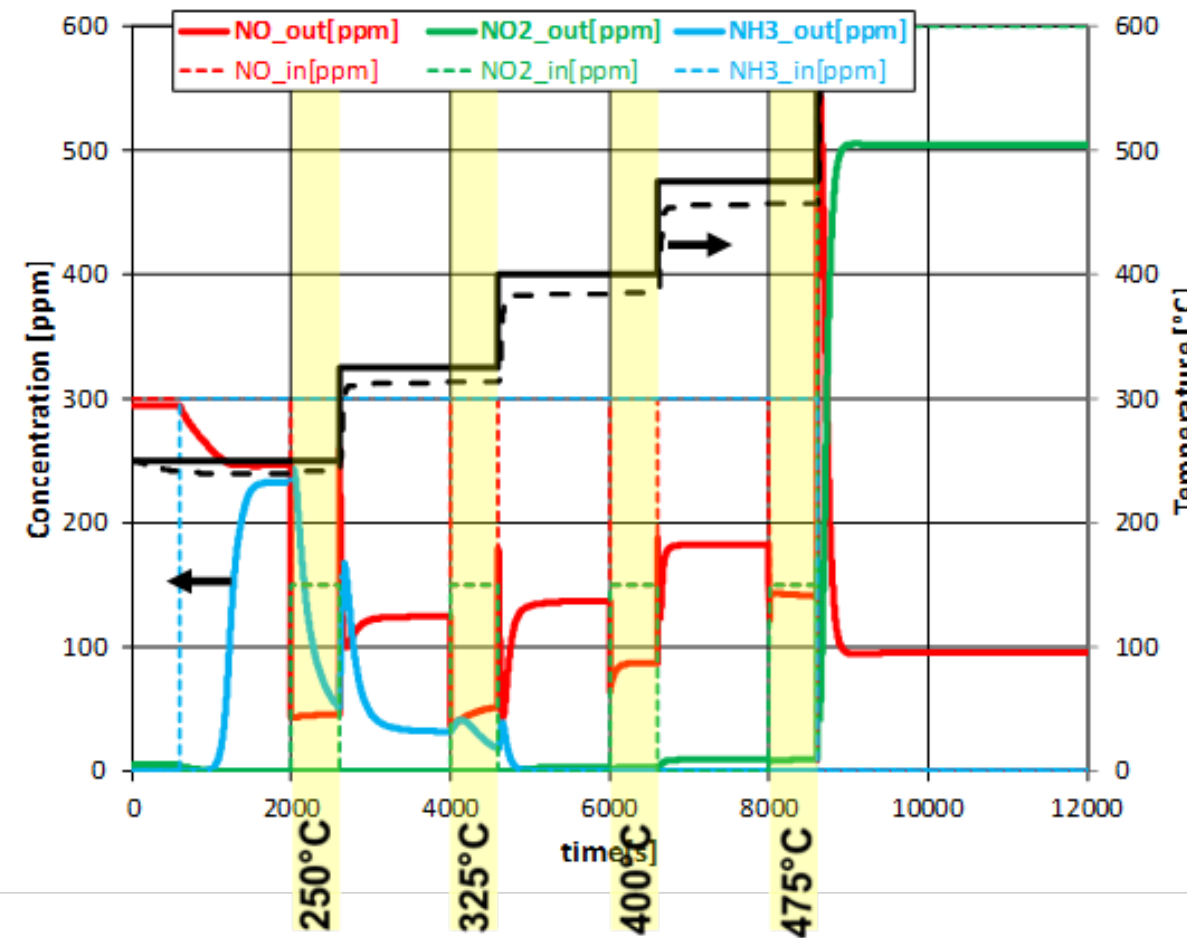
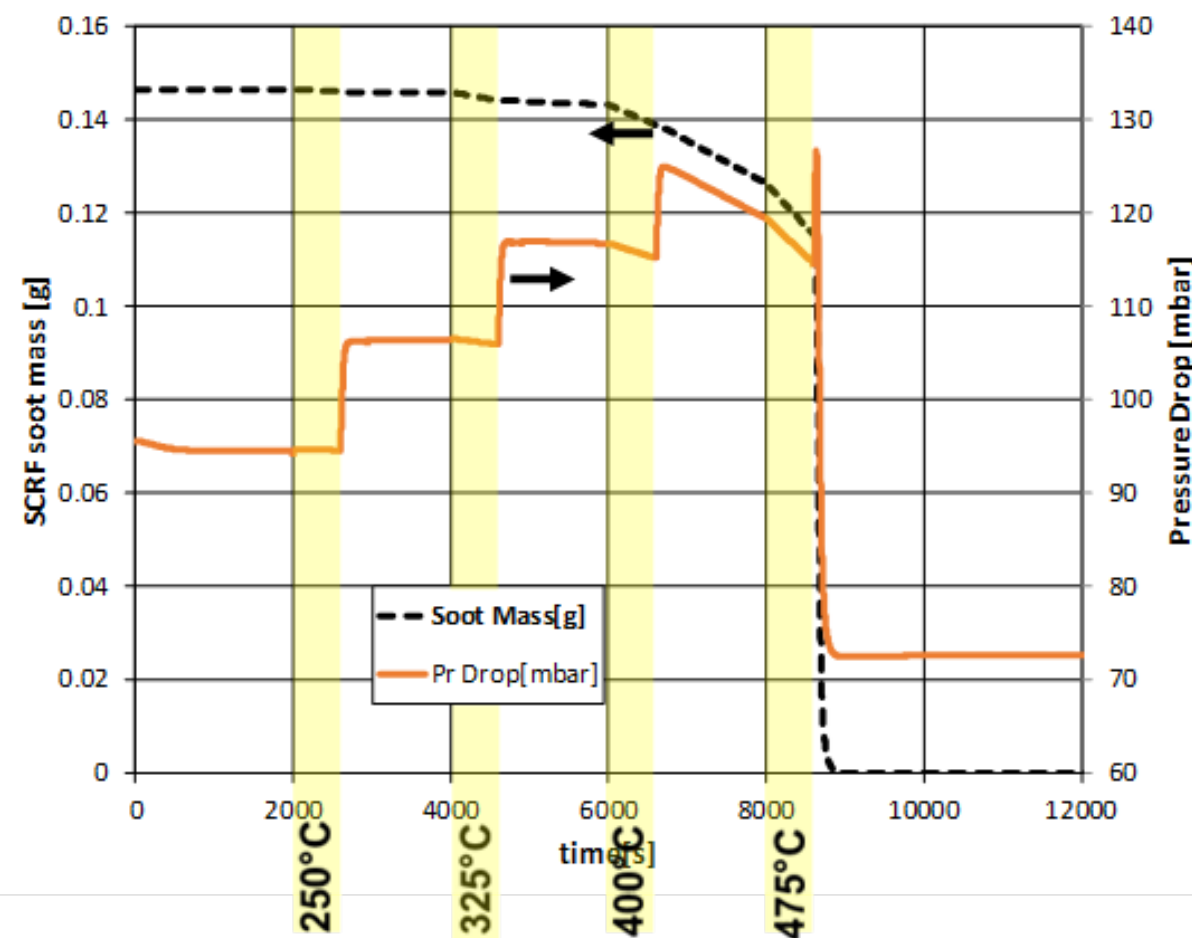
## Axisuite Modeling Configuration



- 4 g/L initial soot loading
- 70 g/L impregnated washcoat loading
- Cu-zeolite Eley-Rideal kinetic scheme

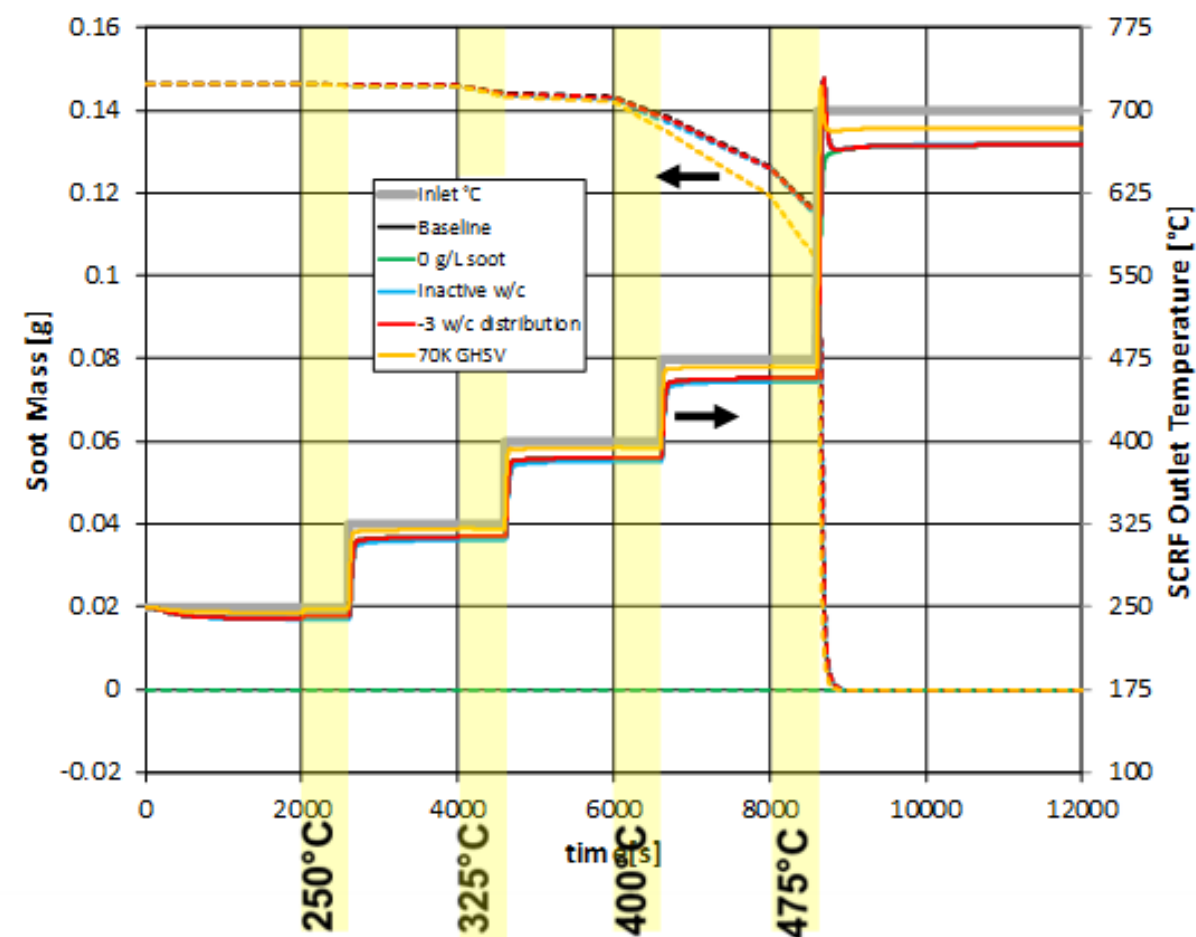
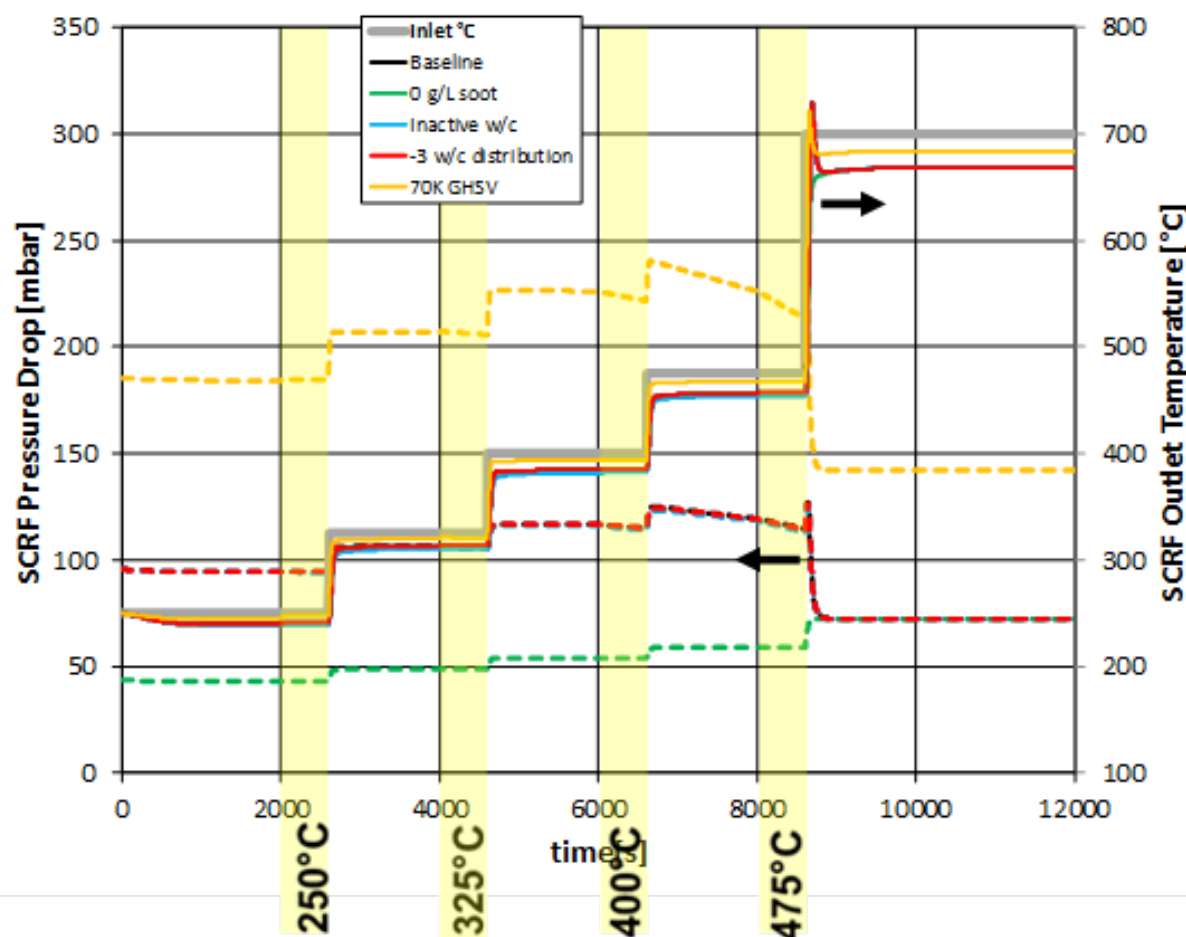


# Axisuite modeling has utility for relating soot oxidation activity and SCR performance



- <insert comment>

# Axisuite modeling has utility for tracking soot oxidation via soot mass and pressure drop



- <insert comment>